

APPENDIX
Selected Hydraulic Piston Cores Plus Reflection
Profiles, Leg 70¹

T. E. Chase, U.S. Geological Survey, Menlo Park, California
 B. J. Long and P. E. Borella,² Deep Sea Drilling Project,
 Scripps Institution of Oceanography, La Jolla, California
 and

J. D. Young and B. A. Seekins, U.S. Geological Survey,
 Menlo Park, California³

The Deep Sea Drilling Project—International Phase of Ocean Drilling (DSDP-IPOD), funded by the National Science Foundation and operated by the University of California, conducted Leg 70 in the area of the Galapagos Spreading Center during November and December, 1979. (A trackline map and navigation listing are included as appendix Fig. 1 and Table 1, respectively. See also Fig. 1 text, this chapter, for general site locality map and detailed surveys.) During this cruise, the newly developed hydraulic piston corer (HPC) was used to recover undisturbed sequences of unconsolidated pelagic and hydrothermal sediments. Recovery averaged 93%, which was attributed to the low shear strength of the sediments and to calm seas. If one eliminates the first hole, Hole 506, recovery averaged a remarkable 98%. (The operation of the hydraulic piston corer is discussed earlier in this chapter; see, in particular, Fig. 6, text.)

The Pacific-Arctic Branch of Marine Geology of the U.S. Geological Survey has built a continuous flow camera for photographing marine cores onto a 35-mm frameless, positive color, microfilm strip. In addition, a microfilm enlargement and retrieval unit was developed at the Branch in order to project the images from microfilm onto reproducible stable base material (mylar). Plates 1 and 2, which are to be found in the back pocket to this volume, reproduce the underway seismic profiles of Leg 70 as they are recorded on the microfilm system and illustrate the quality of the hydraulic piston cores from Sites 506-510. (More detailed investigations can be made from the microfilm copy.)^{4,5}

The core photography was done by placing one-half of the core into a modified "D"-tube tray with a centimeter scale along the side. A conveyer system synchronously moves the tray under the core flow camera while continuous 35-mm color positive microfilm strips are exposed. The underway seismic profiles were also filmed onto continuous 35-mm microfilm but not in color. The color photographs in Plate 2 are from contact duplicates of the original microfilm. The

underway seismic profile strip mounts were made from 35-mm microfilm by setting the microfilm enlargement and retrieval unit to a 3-inch enlargement.

Detailed descriptions of the cores along with their stratigraphic relations are discussed in the chapter by Borella on lithostratigraphy of the Galapagos hydrothermal mounds sediments, this volume.

Trackline Map Leg 70

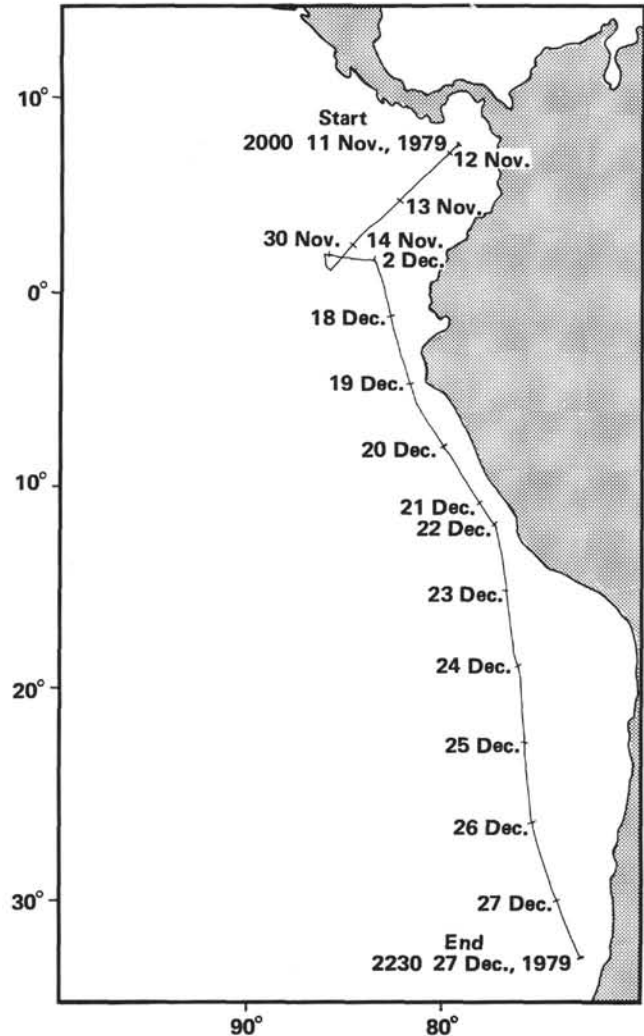


Figure 1. Trackline map, Leg 70.

¹ Jointly prepared by Department of the Interior, U.S. Geological Survey; JOIDES; and Deep Sea Drilling Project, Scripps Institution of Oceanography.

² Present address: Saddleback College, Mission Viejo, California.

³ Assisted by C. P. Miller and C. Larkin of the U.S. Geological Survey; W. Mills, R. Myers, C. Hallman, K. Sanderson, K. Thompson, and J. LeClaire, Deep Sea Drilling Project; and S. M. Smith, D. A. Newhouse, U. G. Albright, and V. W. Psaropoulos, Geologic Data Center, Scripps Institution of Oceanography.

⁴ Equipment used to generate this material: hydraulic piston corer, developed by S. T. Serocki, M. A. Storms, and D. H. Cameron; continuous flow core camera, developed by T. E. Chase and J. D. Young; and microfilm enlargement and retrieval unit ("contraption"), developed by T. E. Chase and J. D. Young.

⁵ Additional information about the data presented here and in back pocket plates 1 and 2 may be obtained from Information Handling Group, Deep Sea Drilling Project, A-031, Scripps Institution of Oceanography, La Jolla, CA 92093.

Table 1. Navigation listing, Leg 70.

DA	MO	YR	TIME	LATITUDE DEG MIN	LONGITUDE DEG MIN	DIST	ACTUAL SPEED CSE	DRIFT SPEED DEG	DR SPEED CSE	CMNT	DRIFT DIST	DRIFT TIME	NO.
1	12	1979	1640	1 24.4	-85 7.4	717.5	10.6 98	1.2 115	9.5 96	C/C			179
1	12	1979	1947	1 22.7	-84 55.6	729.4	10.6 97	1.2 115	9.5 95	C/C			180
2	12	1979	0 1	1 14.4	-83 49.8	795.7	10.6 97	1.2 115	9.5 95				181
2	12	1979	* 035	1 13.60	-83 43.80	801.7	10.8 95	1.3 93	9.5 95	504B	10.3	8.5	183
2	12	1979	035	1 13.6	-83 43.8	801.7	1.3 93	1.3 93	0.0 500	STOP			184
2	12	1979	* 156	1 13.50	-83 42.10	803.4	0.0 273	0.0 273	0.0 500	SATL	1.8	1.3	186
17	12	1979	* 557	1 13.60	-83 43.80	805.1	0.1 122	0.1 122	0.0 500	DEP	1.8	364.0	188
17	12	1979	557	1 13.6	-83 43.8	805.1	6.1 179	0.1 122	6.0 180	U/W			189
17	12	1979	7 6	1 6.6	-83 43.7	812.1	9.6 162	0.1 122	9.5 163	C/C			190
17	12	1979	*1020	0 37.00	-83 34.30	843.2	9.4 162	0.1 41	9.5 163	SATL	0.7	4.4	192
17	12	1979	*1258	0 13.30	-83 26.80	868.1	9.2 164	0.4 322	9.5 163	SATL	0.3	2.6	194
17	12	1979	1420	0 1.3	-83 23.3	880.6	9.2 166	0.4 322	9.5 165	C/C			195
17	12	1979	*1444	0 -2.39	-83 22.40	884.3	9.5 165	0.1 286	9.5 165	SATL	0.7	1.8	197
17	12	1979	*1720	0-26.19	-83 16.20	908.9	9.9 164	0.4 151	9.5 165	SATL	0.2	2.6	199
17	12	1979	*20 2	0-51.99	-83 9.00	935.6	9.8 164	0.4 127	9.5 165	SATL	1.2	2.7	201
17	12	1979	*2146	-1 8.20	-83 4.20	952.6	10.0 164	0.5 136	9.5 165	SATL	0.7	1.7	203
18	12	1979	0 1	-1 29.7	-82 57.8	975.0	10.0 164	0.5 136	9.5 165				204
18	12	1979	* 218	-1 51.50	-82 51.40	997.8	9.7 165	0.2 152	9.5 165	SATL	2.4	4.5	206
18	12	1979	* 728	-2 40.00	-82 38.10	1048.1	9.1 163	0.5 27	9.5 165	SATL	1.3	5.2	208
18	12	1979	* 910	-2 54.80	-82 33.50	1063.6	9.4 164	0.2 17	9.5 165	SATL	1.0	1.7	210
18	12	1979	*1352	-3 37.20	-82 21.70	1107.6	9.0 169	0.8 298	9.5 165	SATL	0.8	4.7	212
18	12	1979	1425	-3 42.1	-82 20.7	1112.5	8.9 162	0.8 298	9.5 159	C/C			213
18	12	1979	*1818	-4 15.10	-82 10.10	1147.2	8.7 166	1.4 286	9.5 159	SATL	3.4	4.4	215
18	12	1979	*2040	-4 35.20	-82 5.20	1167.9	8.8 161	0.8 315	9.5 159	SATL	3.3	2.4	217
18	12	1979	21 9	-4 39.2	-82 3.8	1172.2	8.8 156	0.8 315	9.5 154	C/C			218
19	12	1979	0 1	-5 2.1	-81 53.4	1197.3	8.8 156	0.8 315	9.5 154				219
19	12	1979	* 126	-5 13.40	-81 48.30	1209.7	8.8 155	0.7 322	9.5 154	SATL	3.8	4.8	221
19	12	1979	156	-5 17.4	-81 46.4	1214.1	8.8 157	0.7 322	9.5 156	C/C			222
19	12	1979	* 314	-5 28.00	-81 41.90	1225.6	9.2 157	0.4 306	9.5 156	SATL	1.3	1.8	224
19	12	1979	* 4 8	-5 35.60	-81 38.70	1233.9	9.2 157	0.3 307	9.5 156	SAT	0.4	0.9	226
19	12	1979	440	-5 40.1	-81 36.8	1238.8	9.2 159	0.3 307	9.5 158	C/C			227
19	12	1979	* 556	-5 51.00	-81 32.60	1250.4	8.9 160	0.7 310	9.5 158	SATL	0.7	1.8	229
19	12	1979	615	-5 53.7	-81 31.6	1253.2	8.9 150	0.7 310	9.5 149	C/C			230
19	12	1979	* 8 8	-6 8.20	-81 23.30	1270.0	9.9 151	0.6 197	9.5 149	SATL	1.5	2.2	232
19	12	1979	* 940	-6 21.50	-81 16.00	1285.1	8.5 152	1.0 307	9.5 149	SATL	0.9	1.5	234
19	12	1979	*1258	-6 46.30	-81 2.50	1313.3	8.6 151	0.9 312	9.5 149	SATL	3.5	3.3	236
19	12	1979	*1542	-7 6.90	-80 50.90	1334.9	8.7 151	0.9 306	9.5 149	SATL	2.6	2.7	238
19	12	1979	*1726	-7 20.10	-80 43.60	1352.0	9.3 151	0.4 273	9.5 149	SATL	1.6	1.7	240
19	12	1979	*1936	-7 37.70	-80 33.80	1372.1	9.6 151	0.4 226	9.5 149	SATL	0.9	2.2	242
19	12	1979	2012	-7 42.8	-80 31.0	1377.8	9.6 149	0.4 226	9.5 147	C/C			243
19	12	1979	2025	-7 44.5	-80 29.9	1379.9	9.9 230	0.4 226	9.5 230	C/C			244
19	12	1979	2045	-7 46.7	-80 32.5	1383.2	9.6 149	0.4 226	9.5 147	C/C			245
19	12	1979	*2118	-7 51.20	-80 29.80	1388.5	9.5 145	0.3 59	9.5 147	SATL	0.7	1.7	247
19	12	1979	2148	-7 55.1	-80 27.0	1393.2	9.5 142	0.3 59	9.5 144	C/C			248
20	12	1979	0 1	-8 11.7	-80 13.9	1414.4	9.5 142	0.3 59	9.5 144				249
20	12	1979	* 015	-8 13.50	-80 12.50	1416.6	8.5 144	1.0 322	9.5 144	DR	1.1	3.0	251
20	12	1979	015	-8 13.5	-80 12.5	1416.6	8.5 144	1.0 322	9.5 144				252
20	12	1979	020	-8 14.1	-80 12.1	1417.3	8.5 144	1.0 322	9.5 144				253
21	12	1979	11 9	-12 14.3	-77 16.6	1713.1	1.0 322	1.0 322	0.0 500				254
22	12	1979	027	-12 3.8	-77 25.1	1726.5	7.8 162	1.0 322	8.7 160	U/W			255
22	12	1979	* 516	-12 39.40	-77 13.50	1763.8	8.5 161	0.3 296	8.7 160	SATL	53.2	53.0	257
22	12	1979	* 956	-13 16.90	-77 0.60	1803.4	8.7 161	0.2 236	8.7 160	SATL	1.5	4.7	259
22	12	1979	1019	-13 20.1	-76 59.5	1806.7	8.8 168	0.2 236	8.7 167	C/C			260
22	12	1979	*12 6	-13 35.40	-76 56.20	1822.4	8.8 170	0.5 246	8.7 167	SATL	0.5	2.2	262
22	12	1979	*1352	-13 50.70	-76 53.40	1837.9	8.6 168	0.2 295	8.7 167	SATL	0.9	1.8	264
22	12	1979	1424	-13 55.2	-76 52.4	1842.5	8.6 171	0.2 295	8.7 170	C/C			265
22	12	1979	*1458	-14 0.00	-76 51.60	1847.4	8.8 169	0.1 132	8.7 170	SATL	0.2	1.1	267
22	12	1979	*1646	-14 15.60	-76 48.60	1863.3	8.9 173	0.6 238	8.7 170	SATL	0.3	1.8	269
22	12	1979	*1944	-14 41.90	-76 45.40	1889.7	9.0 174	0.8 236	8.7 170	SATL	1.7	3.0	271
22	12	1979	*2130	-14 57.80	-76 43.80	1905.7	9.0 172	0.4 210	8.7 170	SATL	1.4	1.8	273
22	12	1979	2245	-15 8.9	-76 42.1	1917.0	9.3 169	0.4 210	9.0 167	C/C			274
23	12	1979	0 0	-15 20.3	-76 39.7	1928.6	9.3 169	0.4 210	9.0 167				275
23	12	1979	* 136	-15 34.90	-76 36.70	1943.4	9.3 171	0.6 230	9.0 167	SATL	1.7	4.1	277
23	12	1979	* 244	-15 45.30	-76 34.90	1954.0	9.5 170	0.7 208	9.0 167	SATL	0.8	1.1	279
23	12	1979	* 428	-16 1.50	-76 31.80	1970.5	9.2 170	0.5 241	9.0 167	SATL	1.2	1.7	281
23	12	1979	* 7 0	-16 24.40	-76 27.70	1993.7	9.2 168	0.2 197	9.0 167	SATL	1.4	2.5	283
23	12	1979	* 846	-16 40.30	-76 24.10	2010.0	9.6 167	0.6 160	9.0 167	SATL	0.5	1.8	285
23	12	1979	* 922	-16 45.90	-76 22.70	2015.7	9.4 170	0.6 216	9.0 167	SATL	0.4	0.6	287
23	12	1979	*1110	-17 2.50	-76 19.50	2032.6	9.4 169	0.6 211	9.0 167	SATL	1.0	1.8	289
23	12	1979	*13 0	-17 19.50	-76 16.20	2049.9	9.6 170	0.8 211	9.0 167	SATL	1.1	1.8	291
23	12	1979	*1742	-18 3.80	-76 8.20	2094.8	9.6 171	0.9 219	9.0 167	SATL	3.7	4.7	293
23	12	1979	*2020	-18 28.80	-76 4.20	2120.1	9.0 171	0.6 259	9.0 167	SATL	2.5	2.6	295
23	12	1979	*2110	-18 36.20	-76 2.90	2127.6	9.5 172	1.0 231	9.0 167	SATL	0.5	0.8	297
23	12	1979	*2258	-18 53.10	-76 0.50	2144.7	9.5 171	0.8 224	9.0 167	SATL	1.8	1.8	299
23	12	1979	2319	-18 56.4	-76 0.0	2148.0	9.4 169	0.8 224	8.9 165	C/C			300
24	12	1979	0 0	-19 2.7	-75 58.7	2154.4	9.5 169	0.8 224	9.0 165				301
24	12	1979	* 046	-19 9.80	-75 57.30	2161.7	9.4 168	0.7 218	9.0 165	SATL	1.6	1.8	303
24	12	1979	* 232	-19 26.10	-75 53.70	2178.3	9.6 168	0.8 212	9.0 165	SATL	1.2	1.8	305
24	12	1979	* 340	-19 36.70	-75 51.40	2189.1	9.3 167	0.4 205	9.0 165	SATL	0.9	1.1	307
24	12	1979	7 0	-20 6.9	-75 43.8	2220.2	9.4 171	0.4 205	9.1 170	C/C			308
24	12	1979	* 834	-20 21.50	-75 41.40	2234.9	9.0 172	0.4 280	9.1 170	SATL	2.0	4.9	310
24	12	1979	* 922	-20 28.60	-75 40.40	2242.1	9.1 173	0.4 265	9.1 170	SATL	0.4	0.8	312
24	12	1979	*1020	-20 37.30	-75 39.20	2250.9	9.6 171	0.5 184	9.1 170	SATL	0.5	1.0	314
24	12	1979	*12 5	-20 53.80	-75 36.30	2267.6	9.3 169	0.2 145	9.1 170	SATL	0.9	1.8	316
24	12	1979	1245	-20 59.9	-75 35.1	2273.8	9.3 170	0.2 145	9.1 171	C/C			317
24	12	1979	*1354	-21 10.40	-75 33.20	2284.4	10.0 171	0.9 172	9.1 171	SATL	0.4	1.8	319
24	12	1979	1415	-21 13.9	-75 32.6	2288.0	10.0 172	0.9 172	9.1 172	C/C			320
24	12	1979	*15 0	-21 21.30	-75 31.50	2295.5	8.9 172	0.2 338	9.1 172	SATL	1.0	1.1	322
24	12	1979	1525	-21 25.0	-75 31.0	2299.2	9.0 174	0.2 338	9.1 174	C/C			323
24	12	1979	*1650										

Table 1. (Continued).

DA	MO	YR	TIME	LATITUDE		LONGITUDE		DIST	ACTUAL		DRIFT		DR		DRIFT		NO.	
				DEG	MIN	DEG	MIN		SPEED	CSE	SPEED	HED	SPEED	CSE	CMNT	DIST		TIME
11	11	1979	*1954	7	13.00	-79	46.20	0.0	8.8	214	1.4	152	8.2	223	DR	0.0	0.0	3
11	11	1979	20 5	7	11.7	-79	47.1	1.6	8.8	214	1.4	152	8.2	223	U/W			4
11	11	1979	2225	6	54.8	-79	58.7	22.1	1.4	152	1.4	152	0.0	500	STDP			5
12	11	1979	*035	6	52.1	-79	57.3	25.1	9.1	215	1.4	152	8.5	223	U/W			6
12	11	1979	*043	6	51.10	-79	58.00	26.3	9.3	228	1.1	267	8.5	223	DR	6.8	4.8	8
12	11	1979	053	6	50.1	-79	59.2	27.9	9.6	227	1.1	267	8.8	223	C/S			9
12	11	1979	*314	6	34.80	-80	15.90	50.4	9.4	222	0.7	204	8.8	223	SATL	2.8	2.5	11
12	11	1979	350	6	30.6	-80	19.7	56.1	9.4	223	0.7	204	8.8	225	C/C			12
12	11	1979	*458	6	22.80	-80	27.10	66.8	9.5	224	0.7	216	8.8	225	SATL	1.2	1.7	14
12	11	1979	*734	6	5.10	-80	44.50	91.5	9.4	225	0.6	230	8.8	225	SATL	1.9	2.6	16
12	11	1979	*922	5	53.20	-80	56.60	108.5	9.8	224	1.0	219	8.8	225	SATL	1.1	1.8	18
12	11	1979	*11 2	5	41.50	-81	8.10	124.8	9.1	223	0.4	179	8.8	225	SATL	1.8	1.7	20
12	11	1979	*1712	5	0.50	-81	46.60	181.0	8.7	225	0.1	88	8.8	225	SATL	2.7	6.2	22
12	11	1979	*19 0	4	49.30	-81	57.70	196.7	7.9	224	0.9	55	8.8	225	SATL	0.2	1.8	24
12	11	1979	*21 0	4	37.90	-82	8.70	212.5	8.0	225	0.8	46	8.8	225	SATL	1.9	2.0	26
12	11	1979	*2226	4	29.80	-82	16.80	223.9	8.1	223	0.8	70	8.8	225	SATL	1.2	1.4	28
13	11	1979	0 1	4	20.4	-82	25.5	236.7	8.1	223	0.8	70	8.8	225				29
13	11	1979	*012	4	19.30	-82	26.50	238.2	8.2	225	0.6	48	8.8	225	SATL	1.5	1.8	31
13	11	1979	*4 8	3	56.40	-82	49.30	270.5	8.4	223	0.5	82	8.8	225	SATL	2.4	3.9	33
13	11	1979	*448	3	52.30	-82	53.10	276.1	8.4	224	0.5	62	8.8	225	SATL	0.4	0.7	35
13	11	1979	*556	3	45.50	-82	59.70	285.5	8.9	225	0.1	220	8.8	225	SATL	0.6	1.1	37
13	11	1979	*634	3	41.50	-83	3.70	291.2	8.5	222	0.5	97	8.8	225	SATL	0.1	0.6	39
13	11	1979	*656	3	39.20	-83	5.80	294.3	8.1	223	0.7	67	8.8	225	SATL	0.2	0.4	41
13	11	1979	*832	3	29.70	-83	14.70	307.3	8.2	225	0.6	49	8.8	225	SATL	1.2	1.6	43
13	11	1979	9 0	3	27.0	-83	17.4	311.1	8.2	227	0.6	49	8.8	227	C/C			44
13	11	1979	*1142	3	11.80	-83	33.60	333.3	8.0	231	1.0	13	8.8	227	SATL	1.9	3.2	46
13	11	1979	*1544	2	51.60	-83	58.70	365.5	8.0	230	1.0	20	8.8	227	SATL	4.2	4.0	48
13	11	1979	16 6	2	49.7	-84	0.9	368.4	7.9	228	1.0	20	8.8	225	C/C			49
13	11	1979	*1732	2	42.10	-84	9.40	379.8	7.8	229	1.1	16	8.8	225	SATL	1.8	1.8	51
13	11	1979	*23 4	2	13.60	-84	42.20	423.2	8.1	230	1.0	0	8.8	225	SATL	6.2	5.5	53
14	11	1979	030	2	6.1	-84	51.1	434.9	8.0	221	1.0	0	8.8	217	C/C			54
14	11	1979	033	2	5.8	-84	51.4	435.3	7.7	221	1.0	0	8.5	217	C/S			55
14	11	1979	*052	2	4.00	-84	53.00	437.7	7.2	222	1.4	11	8.5	217	SATL	1.9	1.8	57
14	11	1979	*318	1	50.90	-85	4.80	455.3	7.8	219	0.7	11	8.5	217	SATL	3.5	2.4	59
14	11	1979	345	1	48.2	-85	7.0	458.9	7.5	217	0.7	11	8.2	215	C/C/S			60
14	11	1979	*5 2	1	40.50	-85	12.90	468.5	7.6	219	0.8	352	8.2	215	SATL	1.3	1.7	62
14	11	1979	530	1	37.7	-85	15.1	472.1	7.4	221	0.8	352	8.0	217	C/C/S			63
14	11	1979	*538	1	37.00	-85	15.80	473.1	7.1	219	0.9	21	8.0	217	SATL	0.5	0.6	65
14	11	1979	6 0	1	35.0	-85	17.4	475.7	6.6	219	0.9	21	7.5	217	C/S			66
14	11	1979	*6 8	1	34.30	-85	18.00	476.5	6.9	221	0.8	4	7.5	217	SATL	0.5	0.5	68
14	11	1979	628	1	32.6	-85	19.5	478.8	6.9	222	0.8	4	7.5	218	C/C			69
14	11	1979	*726	1	27.60	-85	23.90	485.5	7.8	227	1.2	299	7.5	218	SATL	1.1	1.3	71
14	11	1979	*744	1	26.00	-85	25.60	487.8	7.1	224	0.8	338	7.5	218	SATL	0.4	0.3	73
14	11	1979	746	1	25.8	-85	25.8	488.1	6.6	223	0.8	338	7.0	217	C/C/S			74
14	11	1979	*1032	1	12.50	-85	38.30	506.3	6.9	223	0.7	314	7.0	217	SATL	2.4	2.8	76
14	11	1979	1055	1	10.6	-85	40.1	509.0	6.9	222	0.7	314	7.0	216	C/C			77
14	11	1979	11 5	1	9.7	-85	40.9	510.2	5.9	223	0.7	314	6.0	216	C/S			78
14	11	1979	*1218	1	4.40	-85	45.80	517.4	6.1	222	0.7	299	6.0	216	SATL	1.3	1.8	80
14	11	1979	1238	1	2.9	-85	47.2	519.4	6.1	221	0.7	299	6.0	214	C/C			81
14	11	1979	1445	0	53.1	-85	55.6	532.3	6.1	219	0.7	299	6.0	212	C/C			82
14	11	1979	1517	0	50.5	-85	57.6	535.6	6.1	217	0.7	299	6.0	210	C/C			83
14	11	1979	1520	0	50.3	-85	57.8	535.9	6.0	215	0.7	299	6.0	208	C/C			84
14	11	1979	1619	0	45.4	-86	1.1	541.8	6.1	217	0.7	299	6.0	210	C/C			85
14	11	1979	1631	0	44.5	-86	1.9	543.0	6.0	213	0.7	299	6.0	206	C/C			86
14	11	1979	17 0	0	42.0	-86	3.4	545.9	6.5	212	0.7	299	6.5	206	C/S			87
14	11	1979	*1710	0	41.10	-86	4.00	547.0	6.5	206	0.0	341	6.5	206	SATL	3.4	4.9	89
14	11	1979	1740	0	38.2	-86	5.4	550.2	6.5	175	0.0	341	6.5	175	C/C			90
14	11	1979	18 0	0	36.0	-86	5.2	552.4	0.0	341	0.0	341	0.0	500	STDP			91
15	11	1979	*18 0	0	36.50	-86	5.40	552.9	0.0	0	0.0	0	0.0	500	S506	0.6	24.8	93
16	11	1979	*130	0	36.50	-86	5.40	552.9	0.0	0	0.0	0	0.0	500	S506A	0.1	7.5	95
16	11	1979	*415	0	36.60	-86	5.40	553.0	0.0	180	0.0	180	0.0	500	S506B	0.1	2.8	97
16	11	1979	*1525	0	36.40	-86	5.40	553.2	0.0	0	0.0	0	0.0	500	S506C	0.2	11.2	99
17	11	1979	*150	0	36.40	-86	5.40	553.2	0.0	0	0.0	0	0.0	500	S506D	0.1	10.4	101
18	11	1979	*093	0	36.50	-86	5.40	553.3	0.0	0	0.0	0	0.0	500	S506E	0.1	23.7	103
18	11	1979	*1230	0	36.60	-86	5.40	553.4	0.0	180	0.0	180	0.0	500	S506F	0.1	11.0	105
18	11	1979	*15 0	0	36.50	-86	5.40	553.5	0.0	180	0.0	180	0.0	500	S506G	0.1	2.5	107
19	11	1979	*1 0	0	36.40	-86	5.40	553.6	0.0	0	0.0	0	0.0	500	S506H	0.1	10.0	109
19	11	1979	*725	0	36.40	-86	5.40	553.6	0.2	180	0.2	180	0.0	500	S506I	0.1	6.4	111
19	11	1979	*1930	0	34.00	-86	5.40	556.0	0.0	90	0.0	90	0.0	500	S507	2.4	12.1	113
20	11	1979	*1711	0	34.00	-86	5.30	556.1	0.0	0	0.0	0	0.0	500	S507A	0.1	21.7	115
20	11	1979	*19 3	0	34.00	-86	5.30	556.1	0.0	0	0.0	0	0.0	500	S507B	0.1	1.9	117
21	11	1979	*734	0	34.00	-86	5.30	556.1	0.0	180	0.0	180	0.0	500	S507C	0.1	12.5	119
21	11	1979	*1232	0	33.90	-86	5.30	556.2	0.0	0	0.0	0	0.0	500	S507D	0.2	29.0	121
22	11	1979	*2315	0	33.90	-86	5.30	556.2	0.0	0	0.0	0	0.0	500	S507E	0.1	10.7	123
23	11	1979	*130	0	33.90	-86	5.30	556.2	0.0	270	0.0	270	0.0	500	S507F	0.1	2.3	125
23	11	1979	*1130	0	33.90	-86	5.40	556.3	0.1	135	0.1	135	0.0	500	S507G	0.1	10.0	127
23	11	1979	*1315	0	33.80	-86	5.30	556.4	0.0	0	0.0	0	0.0	500	S507H	0.2	1.8	129
23	11	1979	*2215	0	33.80	-86	5.30	556.4	0.3	211	0.3	211	0.0	500	S507I	0.1	9.0	131
24	11	1979	*522	0	32.00	-86	6.40	558.5	0.0	0	0.0	0</						

Table 1. (Continued).

DA	MO	YR	TIME	LATITUDE		LONGITUDE		DIST	ACTUAL		DRIFT		DR		CMNT	DRIFT		NO.
				DEG	MIN	DEG	MIN		SPEED	CSE	SPEED	HED	SPEED	CSE		DIST	TIME	
25	12	1979	*2125	-25	54.00	-74	59.10	2570.0	8.9	167	0.4	56	9.1	170	SATL	3.4	7.2	352
25	12	1979	22 0	-25	59.1	-74	57.8	2575.2	9.0	159	0.4	56	9.1	162	C/C			353
26	12	1979	0 0	-26	15.9	-74	50.8	2593.2	9.0	159	0.4	56	9.1	162				354
26	12	1979	* 235	-26	37.60	-74	41.60	2616.4	8.9	164	0.3	293	9.1	162	SATL	2.3	5.2	356
26	12	1979	320	-26	44.0	-74	39.5	2623.1	8.9	165	0.3	293	9.1	163	C/C			357
26	12	1979	* 7 6	-27	16.30	-74	29.50	2656.6	8.9	169	0.9	267	9.1	163	SATL	1.5	4.5	359
26	12	1979	* 842	-27	30.30	-74	26.40	2670.8	9.4	165	0.4	213	9.1	163	SATL	1.6	1.6	361
26	12	1979	9 6	-27	33.9	-74	25.3	2674.6	8.8	163	0.4	213	8.5	161	C/C/S			362
26	12	1979	*1028	-27	45.40	-74	21.40	2686.6	8.8	160	0.3	142	8.5	161	SATL	0.8	1.8	364
26	12	1979	*1210	-27	59.50	-74	15.70	2701.6	9.3	159	0.8	142	8.5	161	SATL	0.6	1.7	366
26	12	1979	*1510	-28	25.60	-74	4.50	2729.5	9.5	166	1.2	199	8.5	161	SATL	2.6	3.0	368
26	12	1979	*1655	-28	41.70	-73	59.80	2746.1	9.4	166	1.2	206	8.5	161	SATL	2.2	1.8	370
26	12	1979	*1850	-28	59.20	-73	54.90	2764.1	9.4	161	0.9	161	8.5	161	SATL	2.4	1.9	372
26	12	1979	1910	-29	2.2	-73	53.7	2767.2	9.4	157	0.9	161	8.5	157	C/C			373
26	12	1979	*2220	-29	29.70	-73	40.60	2797.1	9.1	155	0.6	132	8.5	157	SATL	3.3	3.5	375
26	12	1979	2250	-29	33.8	-73	38.4	2801.6	9.2	157	0.6	132	8.6	159	C/C/S			376
26	12	1979	*2358	-29	43.40	-73	33.80	2812.0	8.7	158	0.2	98	8.6	159	SATL	1.1	1.6	378
27	12	1979	0 0	-29	43.7	-73	33.7	2812.3	8.7	158	0.2	98	8.6	159				379
27	12	1979	030	-29	47.7	-73	31.8	2816.6	8.7	160	0.2	98	8.6	161	C/C			380
27	12	1979	142	-29	57.5	-73	27.6	2827.1	8.7	151	0.2	98	8.6	152	C/C			381
27	12	1979	* 146	-29	58.00	-73	27.30	2827.6	8.4	154	0.3	288	8.6	152	SATL	0.4	1.8	383
27	12	1979	7 0	-30	37.2	-73	4.8	2871.4	7.0	154	0.3	288	7.2	152	C/S			384
27	12	1979	* 928	-30	52.60	-72	56.00	2888.5	7.0	154	0.3	275	7.2	152	SATL	2.7	7.7	386
27	12	1979	*1118	-31	4.20	-72	49.50	2901.4	7.4	150	0.3	91	7.2	152	SATL	0.7	1.8	388
27	12	1979	*1420	-31	23.50	-72	36.40	2923.7	8.0	148	1.0	118	7.2	152	SATL	1.0	3.0	390
27	12	1979	1448	-31	26.7	-72	34.1	2927.5	8.0	150	1.0	118	7.2	154	C/C			391
27	12	1979	*16 5	-31	35.60	-72	28.00	2937.8	7.6	155	0.5	177	7.2	154	SATL	1.8	1.8	393
27	12	1979	*1948	-32	1.40	-72	14.10	2966.2	6.8	156	0.5	303	7.2	154	SATL	1.8	3.7	395
27	12	1979	1950	-32	1.6	-72	14.0	2966.4	6.8	155	0.5	303	7.2	153	C/C			396
27	12	1979	*2114	-32	10.20	-72	9.30	2975.9	7.9	153	0.7	154	7.2	153	SATL	0.8	1.4	398
27	12	1979	2114	-32	10.2	-72	9.3	2975.9	6.7	153	0.7	154	6.0	153	C/S			399
27	12	1979	*2134	-32	12.24	-72	8.14	2978.1	6.7	153	0.0	0	6.0	153	SATL	0.3	0.3	400