18. PALEOMAGNETISM AND ACCUMULATION RATES OF SEDIMENTS AT SITES 576 AND 578, DEEP SEA DRILLING PROJECT LEG 86, WESTERN NORTH PACIFIC[1]

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ABSTRACT

The upper sections of Deep Sea Drilling Project Sites 576 (32°21.4′N, 164°16.5′E) and 578 (33°55.6′N, 151°37.7′E) both have stable detrital remanence that can be correlated with the standard reversal stratigraphy. Site 576 contains all reversals above the base of the Gilbert Epoch (5 m.y.) at about 25 m, whereas Site 578 contains a remarkable section of about 60 reversals extending to Anomaly 5B (15 m.y.) at about 150 m sub-bottom depth. In both cases, the paleomagnetic stratigraphy breaks down when accumulation rates drop below 2 m/m.y. At both sites, authigenic manganiferous clays deposited from 70 to 16 m.y. ago accumulated at about 0.4 m/m.y. Similarly, at both sites, the Pleistocene pulse of eolian debris increased accumulation rates by about 6 m/m.y.^{2}. From 16 to 2 m.y. ago, however, sediment accumulated at Site 578 about five times as rapidly as at Site 576, apparently because of augmented input to the western site by bottom currents.

INTRODUCTION

Geologic Setting

Prior paleomagnetic studies of the sediments in the vicinity of Deep Sea Drilling Project (DSDP) Site 576, based on piston cores collected during cruise *Vema*-36 (Barton and Sopher, 1982), have shown that deposition has been extremely uniform (core to core variations in sedimentation rates are only about 6% over 10,000 km^2). In contrast, Site 578 lies close to an east/west boundary across which there is a several-fold increase in sedimentation rate from south to north (Jacobi et al., this volume). Because of the stable remanence of the *Vema*-36 samples and the generally poor preservation of siliceous microfossils, we anticipated that dating of the Leg 86 sections would depend heavily on paleomagnetic stratigraphy. In addition, we were interested in the degree to which the paleomagnetic results from giant piston core LL44-GPC-3, taken north of Hawaii (Fig. 1; Prince et al., 1980) would resemble those at the lithologically similar Site 576, some 40° of longitude to the west.

The lithology of the Site 576 sediments is relatively simple. Above 27 m, the section is dominated by yellow-brown pelagic clay rich in quartz (Leinen, this volume). This clay is terrigenous debris derived from Asia and carried to the site by upper atmosphere westerlies (Janecek, this volume). Similar material dominates late Cenozoic pelagic clays across the Pacific (Leinen and Heath, 1981; Moore and Heath, 1978).

The sediments between 27 and 56 m are very dark brown "slick" clays depleted in quartz and enriched in ferromanganese oxyhydroxides. These clays accumulated very slowly (less than 1 m/m.y.; Doyle and Riedel, this volume) and are dominated by authigenic components (silicates as well as oxyhydroxides). Below 56 m, the clays are interbedded with carbonate ooze derived either from fluctuations in the width of the Late Cretaceous equatorial carbonate zone or from turbidites originating on nearby topographic highs.

The deeper part of the section at Site 578 is comparable to Site 576. Above 77 m, however, the section consists of gray green clay with variable amounts of biogenic silica and numerous thin layers of volcanic ash and dark greenish gray indurated clay that may be altered basic ash. These sediments are reduced (authigenic pyrite is common) and are richer in organic carbon than are the Site 576 deposits.

The yellow-brown clays analogous to the surficial deposits at Site 576 extend from 77 to 125 m. The dark brown "slick" clays complete the section from 125 to 176 m, terminating against chert overlain by a few silicified foraminifers. Unlike Site 576, the basal sediments are not calcareous, suggesting that at Site 578, biogenic sediments (now silicified to chert) gave way abruptly to pelagic clay.

Methodology

Magnetic samples were taken at 10- or 20-cm intervals in visually undisturbed sections of core using a new sampling system designed by R. Karlin. This sampler produces strikingly less disturbance of the magnetic samples and of the surrounding sediment left behind in the core, particularly in stiff clays, than does the conventional technique of pressing 2 × 2 × 2 cm plastic boxes into the split sediment surface. Each sample was extracted from the core with a thin-walled, sharpened, 2 × 2 cm stainless-steel tube. The bottom of the resultant square sample was trimmed of disturbed sediment and extruded into a standard 2 × 2 × 2 cm plastic cube by means of a tightly fitting plastic piston. The cube was trimmed to a flat surface and capped. Sample cubes were grouped into packages of 50, each package being individually wrapped in Saran® wrap, then seawater-saturated paper toweling, then another layer of Saran® wrap to minimize water loss. Packages were shipped back to

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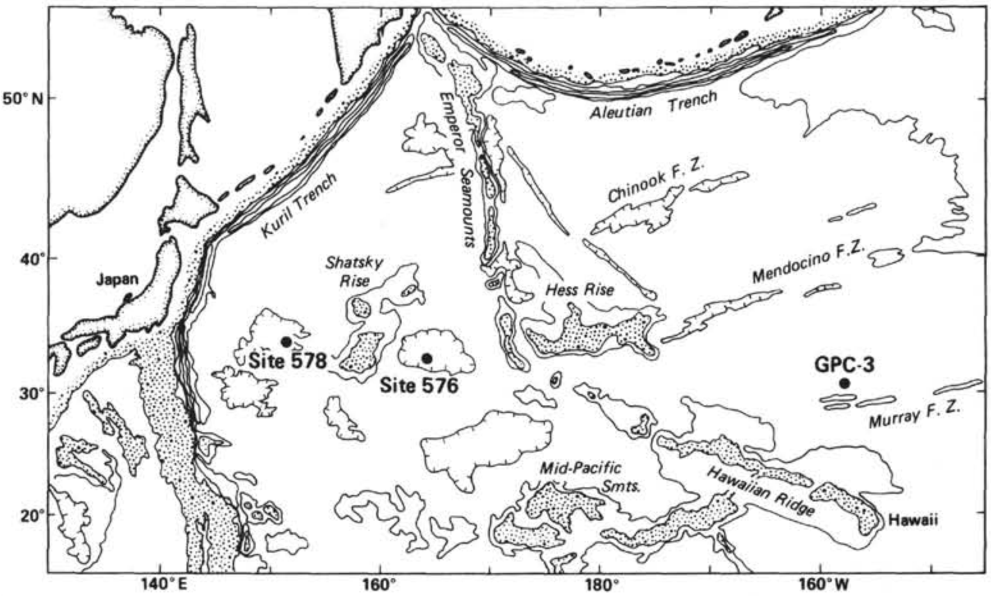

Figure 1. Location of Sites 576 and 578 and giant piston core LL44-GPC-3 relative to the generalized bathymetry of the western North Pacific (after Chase, 1975). Areas shallower than 4 km stippled; 5 km contour plain; 6 km contour hachured.

Oregon State University in carrying cases lined with mu-metal to minimize exposure to extraneous magnetic fields.

Samples were weighed wet (for later water-content determinations) before being subjected to paleomagnetic analysis on a Digico magnetometer. Most samples were run for natural remanent magnetization (NRM), and again after alternating field (AF) demagnetization at 100 and 200 Oe. Where the remanence appeared unstable, additional measurements at higher demagnetization levels (up to 800 Oe in some cases) were taken in an effort to characterize the original detrital remanence. The reported inclinations and declinations are based on the 100-Oe data, or on vector averages of higher demagnetization levels, depending on the behavior of intensities and directions as a function of demagnetization intensity.

RESULTS

Site 576

Tables 1 to 4 list the magnetic data for Holes 576 and 576B. Figure 2 and Table 5 show the polarity profile based on the combined results, versus the latest standard polarity scale of Berggren et al. (in press). The reversal stratigraphy is interpretable through most of the Gilbert Epoch, the base of the Thvera Event being the last reliable boundary.

Most of the reversals were picked on the basis of the inclination data, although confirmed by 180° declination changes. The absolute declinations are unknown because of difficulties with the shipboard core-orienting device and rotation of the hydraulic piston core (HPC) barrel as it is driven ahead of the bit (Fig. 3).

A much more serious problem in constructing Figure 2 arose from the depth discrepancies and the condition of HPC cores from Holes 576 and 576B. The alignment of lithologic as well as magnetic boundaries suggests that Cores 576-2 and 576-3 sampled the same interval and that the top 4 m in Hole 576B was not recovered in Hole 576 (see Site 576 chapter, this volume). In addition, the normally magnetized intervals below the Kaena and Mammoth events are repeated in Core 576B-3, suggesting that the HPC "bounced" while sampling this interval. Such an occurrence, like the presence of "flow-in" structures in some of the cores, is indicative of significant piston motion as the HPC penetrated the sediment. We estimate that about 20% of the core recovered is so deformed as to be stratigraphically suspect. Based on the magnetic and lithologic correlations between Holes 576 and 576B, however, we believe that the composite section of Figure 2 approaches the *in situ* stratigraphy. There is some residual uncertainty about the thickness of the reversed section between the Olduvai Event and the base of the Matuyama Epoch (due to a small interval that lies in the gap between Cores 576-2 and 576-4 and in a disturbed section of Core 576B-2).

Based on the radiolarian stratigraphy (Morley, this volume), neither hole recovered the surficial sediments. The core-top age of 280,000 yr. (Core 576B-1), obtained by extrapolating the polarity stratigraphy (Fig. 2), agrees well with Morley's estimate of 200,000–300,000 yr.

Below 25 m, the reversal stratigraphy becomes uninterpretable. At this depth, the lithology changes from brown to very dark brown clay, and the sedimentation rate drops below 1 m/m.y. The average J_{100}/J_0 value also decreases abruptly (Fig. 4), suggesting that the ratio of magnetically unstable authigenic oxyhydroxides to stable detrital magnetic minerals has become so large that the detrital remanence is submerged in the "noise" of chemical remanence. A similar breakdown in stable remanence at this lithologic boundary has been recorded in other North Pacific cores (Opdyke and Foster, 1970; Kent and Lowrie, 1974; Prince et al., 1980).

The NRM profile (Fig. 4) is noisy at all depths, with a tendency to higher values below about 29 m and more

Table 1. Magnetic properties of samples from Hole 576.

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
1	1	1	11	415	299	58	0.4230E-04	0.3750E-04	0.887	0.3193E-04	0.755	A1-2
3	1	1	31	435	322	49	0.3368E-04	0.2584E-04	0.767	0.2353E-04	0.699	A1-2
5	1	1	51	455	301	53	0.2309E-04	0.2153E-04	0.932	0.1843E-04	0.798	A1-2
6	1	1	61	465	292	46	0.3882E-04	0.2892E-04	0.745	0.3160E-04	0.814	A1-4
7	1	1	71	475	300	58	0.4271E-04	0.3785E-04	0.886	0.3269E-04	0.765	A1-2
9	1	1	91	495	277	57	0.3416E-04	0.2769E-04	0.811	0.2254E-04	0.660	A1-2
11	1	1	111	515	305	48	0.2838E-04	0.2542E-04	0.896	0.2078E-04	0.732	A1-2
13	1	1	131	535	300	56	0.3474E-04	0.3488E-04	1.004	0.2855E-04	0.822	A1-2
14	1	1	141	545	300	58	0.4269E-04	0.3895E-04	0.912	0.3424E-04	0.802	A1-2
15	1	2	6	555	298	-24	0.5103E-04	0.4962E-04	0.972	0.3957E-04	0.776	A1-2
16	1	2	16	565	313	66	0.4576E-04	0.3802E-04	0.831	0.3414E-04	0.746	A1-2
17	1	2	22	575	330	60	0.4128E-04	0.3667E-04	0.888	0.3102E-04	0.751	A1-2
19	1	2	41	595	310	68	0.3731E-04	0.3434E-04	0.920	0.2829E-04	0.758	A1-2
21	1	2	61	615	360	62	0.3926E-04	0.3524E-04	0.897	0.3011E-04	0.767	A1-2
23	1	2	81	635	3	62	0.5004E-04	0.4405E-04	0.880	0.3716E-04	0.743	A1-2
24	1	2	91	645	33	63	0.4049E-04	0.3579E-04	0.884	0.2935E-04	0.725	A1-2
26	1	2	101	655	40	66	0.1771E-04	0.1446E-04	0.816	0.1215E-04	0.686	A1-3
25	1	*	7	668	186	-35	0.2550E-04	0.1928E-04	0.756	0.1476E-04	0.579	A1-2
27	2	1	6	701	263	-54	0.1146E-04	0.1382E-04	1.206	0.1246E-04	1.088	A1-2
29	2	1	26	721	297	-56	0.1599E-04	0.2161E-04	1.351	0.1818E-04	1.137	A1-2
31	2	1	46	741	339	-42	0.2154E-04	0.2321E-04	1.078	0.1857E-04	0.862	A1-2
33	2	1	66	761	21	-53	0.1397E-04	0.1635E-04	1.170	0.1383E-04	0.990	A1-2
35	2	1	86	781	30	-50	0.1191E-04	0.1252E-04	1.051	0.1037E-04	0.871	A1-2
36	2	1	96	791	47	-51	0.2534E-04	0.2473E-04	0.976	0.2016E-04	0.796	A1-4
37	2	1	106	801	44	-47	0.2758E-04	0.2896E-04	1.050	0.2484E-04	0.901	A1-2
39	2	1	126	821	65	-53	0.1371E-04	0.1548E-04	1.129	0.1408E-04	1.027	A1-2
41	2	1	146	841	68	-52	0.2097E-04	0.2631E-04	1.254	0.2079E-04	0.991	A1-2
43	2	2	16	861	97	-51	0.2348E-04	0.2940E-04	1.252	0.2628E-04	1.119	A1-2
44	2	2	26	871	99	-51	0.1848E-04	0.1897E-04	1.026	0.1587E-04	0.859	A1-2
45	2	2	36	881	263	19	0.6239E-05	0.1639E-05	0.263	0.1123E-05	0.180	L3
46	2	2	46	891	292	47	0.1105E-04	0.8203E-05	0.742	0.5910E-05	0.535	A1-2
47	2	2	56	901	273	53	0.2331E-04	0.1953E-04	0.838	0.1553E-04	0.666	A1-2
49	2	2	76	921	278	54	0.2681E-04	0.2425E-04	0.904	0.2130E-04	0.794	A1-4
51	2	2	96	941	302	54	0.4001E-04	0.3572E-04	0.893	0.2886E-04	0.721	A1-2
53	2	2	116	961	267	-38	0.2869E-05	0.6663E-06	0.232	0.5597E-06	0.194	A3-4
55	2	2	136	981	143	-57	0.1954E-04	0.2169E-04	1.110	0.1744E-04	0.893	A1-2
57	2	3	6	1001	163	-53	0.1966E-04	0.2029E-04	1.032	0.1705E-04	0.868	A1-2
59	2	3	26	1021	158	-45	0.2738E-04	0.2710E-04	0.990	0.2090E-04	0.763	A1-2
61	2	3	46	1041	172	-52	0.2014E-04	0.2078E-04	1.032	0.1792E-04	0.890	A1-2
63	2	3	66	1061	173	-65	0.1663E-04	0.1853E-04	1.115	0.1531E-04	0.921	A1-2
65	2	3	86	1081	183	-49	0.1428E-04	0.1609E-04	1.126	0.1311E-04	0.918	A1-2
67	2	3	106	1101	174	-50	0.1109E-04	0.1149E-04	1.037	0.1006E-04	0.907	A1-2
69	2	3	126	1121	171	-49	0.2528E-04	0.2484E-04	0.982	0.2173E-04	0.860	A1-2
71	2	3	146	1141	196	-59	0.2699E-04	0.2627E-04	0.973	0.2315E-04	0.858	A1-2
73	2	4	16	1161	166	-43	0.2324E-04	0.2224E-04	0.957	0.1925E-04	0.828	A1-2
75	2	4	36	1181	170	-51	0.3210E-04	0.3216E-04	1.002	0.2697E-04	0.840	A1-2
77	2	4	56	1201	171	-53	0.1760E-04	0.1838E-04	1.044	0.1541E-04	0.875	A1-2
79	2	4	76	1221	177	-49	0.2970E-04	0.2775E-04	0.934	0.2457E-04	0.827	A1-2
81	2	4	96	1241	180	-56	0.2503E-04	0.2525E-04	1.009	0.2141E-04	0.855	A1-2
83	2	4	116	1261	182	-48	0.2596E-04	0.2720E-04	1.048	0.1986E-04	0.765	A1-2
85	2	4	136	1281	174	-50	0.1689E-04	0.1946E-04	1.152	0.1533E-04	0.907	A1-2
87	2	5	6	1301	172	-46	0.2641E-04	0.2578E-04	0.977	0.2275E-04	0.862	A1-2
89	2	5	26	1321	168	-59	0.2302E-04	0.2427E-04	1.054	0.2055E-04	0.892	A1-2
91	2	5	46	1341	156	-48	0.1699E-04	0.1856E-04	1.092	0.1477E-04	0.869	A1-2
93	2	5	66	1361	159	-51	0.2477E-04	0.2514E-04	1.015	0.2028E-04	0.819	A1-2
95	2	5	86	1381	158	-59	0.1651E-04	0.1850E-04	1.121	0.1448E-04	0.877	A1-2
96	2	5	96	1391	162	-67	0.1218E-04	0.1443E-04	1.185	0.1066E-04	0.875	A1-2
97	2	5	106	1401	287	-69	0.7365E-05	0.1077E-04	1.463	0.8607E-05	1.169	A1-2
98	2	5	116	1411	289	-71	0.2168E-04	0.2138E-04	0.986	0.1733E-04	0.799	A1-2
99	2	5	126	1421	154	-67	0.2143E-04	0.2139E-04	0.998	0.1799E-04	0.840	A1-3

Table 1. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
101	2	5	146	1441	185	-84	0.2224E-04	0.1966E-04	0.884	0.1736E-04	0.781	A1-4
102	2	6	6	1451	249	-68	0.2032E-04	0.2167E-04	1.066	0.1792E-04	0.882	A1-2
103	2	6	16	1461	75	-79	0.2178E-04	0.2120E-04	0.973	0.1739E-04	0.798	A1-3
104	2	6	26	1471	13	-61	0.2460E-04	0.2551E-04	1.037	0.2191E-04	0.891	A1-2
105	2	6	36	1481	254	-43	0.1296E-04	0.1201E-04	0.927	0.1035E-04	0.799	A1-2
106	2	6	46	1491	6	29	0.5678E-05	0.3672E-05	0.647	0.2996E-05	0.528	A1-2
107	2	6	56	1501	343	38	0.5924E-05	0.5729E-05	0.967	0.3919E-05	0.662	A1-2
108	2	6	66	1511	4	34	0.4720E-05	0.4060E-05	0.860	0.2946E-05	0.624	A1-2
109	2	6	76	1521	22	14	0.3792E-05	0.4242E-05	1.119	0.3337E-05	0.880	A1-3
110	2	6	86	1531	20	-20	0.1421E-04	0.1262E-04	0.888	0.9781E-05	0.688	A1-3
111	2	6	96	1541	6	28	0.1448E-04	0.1215E-04	0.839	0.9639E-05	0.666	A1-3
113	2	6	116	1561	329	19	0.9358E-05	0.8217E-05	0.878	0.7149E-05	0.764	A1-3
114	2	6	126	1571	335	19	0.5845E-05	0.5615E-05	0.961	0.3800E-05	0.650	A1-4
115	2	6	136	1581	32	51	0.9028E-05	0.6818E-05	0.755	0.5357E-05	0.593	A1-2
117	2	7	6	1601	352	45	0.1968E-05	0.8114E-06	0.412	0.2353E-06	0.120	A1-2
118	2	7	16	1611	185	-53	0.6332E-05	0.7110E-05	1.123	0.6297E-05	0.994	A1-2
119	2	7	26	1621	198	-56	0.7243E-05	0.6263E-05	0.865	0.3012E-05	0.416	A1-2
121	2	7	46	1641	153	-24	0.2754E-05	0.2717E-05	0.098	0.2156E-05	0.076	A1-2
123	3	1	36	1021	288	-58	0.6702E-05	0.7439E-05	1.110	0.6139E-05	0.916	A1-2
125	3	1	56	1041	285	-49	0.1256E-04	0.2136E-04	1.701	0.2377E-04	1.893	A1-2
127	3	1	76	1061	291	-45	0.6494E-05	0.1676E-04	2.582	0.1343E-04	2.068	A1-2
129	3	1	96	1081	281	-62	0.6616E-05	0.9555E-05	1.444	0.7800E-05	1.179	A1-2
131	3	1	116	1101	278	-38	0.7595E-05	0.1097E-04	1.444	0.8743E-05	1.151	A1-2
133	3	1	136	1121	281	-50	0.2430E-04	0.2407E-04	0.991	0.1989E-04	0.818	A1-2
135	3	2	6	1141	311	-46	0.2001E-04	0.2085E-04	1.042	0.1888E-04	0.944	A1-2
137	3	2	26	1161	296	-57	0.2485E-04	0.2500E-04	1.006	0.2058E-04	0.828	A1-2
139	3	2	46	1181	296	-52	0.2369E-04	0.2498E-04	1.054	0.2210E-04	0.933	A1-2
141	3	2	66	1201	284	-48	0.2149E-04	0.2268E-04	1.055	0.1729E-04	0.804	A1-2
143	3	2	86	1221	291	-47	0.2528E-04	0.2862E-04	1.132	0.2192E-04	0.867	A1-2
145	3	2	106	1241	291	-54	0.1870E-04	0.1957E-04	1.047	0.1581E-04	0.845	A1-2
147	3	2	126	1261	281	-42	0.1428E-04	0.1431E-04	1.003	0.1286E-04	0.901	A1-2
149	3	2	146	1281	261	-58	0.2827E-04	0.2562E-04	0.906	0.2274E-04	0.804	A1-2
151	3	3	16	1301	288	-46	0.2253E-04	0.2372E-04	1.053	0.1883E-04	0.836	A1-2
153	3	3	36	1321	276	-48	0.2109E-04	0.2098E-04	0.995	0.1740E-04	0.825	A1-2
155	3	3	56	1341	268	-57	0.7469E-05	0.1003E-04	1.343	0.7404E-05	0.991	A1-2
157	3	3	76	1361	299	-46	0.1794E-04	0.1956E-04	1.090	0.1515E-04	0.844	A1-2
159	3	3	96	1381	271	-47	0.1753E-04	0.1999E-04	1.140	0.1584E-04	0.904	A1-2
161	3	3	116	1401	275	-50	0.1284E-04	0.1509E-04	1.175	0.1207E-04	0.940	A1-2
163	3	3	136	1421	273	-43	0.1145E-04	0.1195E-04	1.044	0.1064E-04	0.929	A1-2
165	3	4	6	1441	284	-51	0.2897E-04	0.2705E-04	0.934	0.2599E-04	0.897	A1-2
167	3	4	26	1461	273	-53	0.2879E-04	0.2950E-04	1.024	0.2461E-04	0.855	A1-2
169	3	4	56	1491	290	-53	0.1133E-04	0.1379E-04	1.217	0.1078E-04	0.951	A1-2
171	3	4	76	1511	108	42	0.2170E-04	0.1729E-04	0.797	0.1243E-04	0.573	A1-2
173	3	4	46	1481	284	-57	0.1582E-04	0.1582E-04	1.000	0.1309E-04	0.827	A1-2
175	3	4	106	1541	100	56	0.2849E-04	0.2340E-04	0.821	0.1776E-04	0.623	A1-2
177	3	4	126	1561	106	50	0.3383E-04	0.2742E-04	0.811	0.2310E-04	0.683	A1-2
179	3	4	146	1581	162	40	0.5520E-05	0.8473E-06	0.154	0.4673E-06	0.085	A1-3
181	3	5	16	1601	281	-54	0.1680E-04	0.1852E-04	1.102	0.1589E-04	0.946	A1-2
183	3	*	6	1623	187	-68	0.1342E-04	0.1490E-04	1.111	0.1166E-04	0.869	A1-2
185	3	*	26	1643	190	-66	0.2706E-04	0.2808E-04	1.038	0.2276E-04	0.841	A1-2
186	4	1	6				0.9634E-05	0.6745E-05	0.700	0.5242E-05	0.544	F
187	4	1	16				0.1172E-04	0.8100E-05	0.691	0.6435E-05	0.549	F
188	4	1	26				0.1736E-04	0.1196E-04	0.689	0.8915E-05	0.514	F
189	4	1	76	1856			0.6859E-05	0.4927E-05	0.718	0.3259E-05	0.475	U
190	4	1	86	1866	152	38	0.1306E-04	0.5822E-05	0.446	0.4637E-05	0.355	A1-2
191	4	1	96	1876	152	58	0.3089E-04	0.1915E-04	0.620	0.1481E-04	0.479	A1-2
192	4	1	106	1886	146	51	0.3843E-04	0.2746E-04	0.715	0.1952E-04	0.508	A1-4
193	4	1	116	1896	146	55	0.2768E-04	0.2053E-04	0.742	0.1586E-04	0.573	A1-2
194	4	1	126	1906	155	56	0.21100-04	0.13500-04	0.639	0.10100-04	0.478	A1-2
195	4	1	136	1916	143	54	0.2888E-04	0.1922E-04	0.665	0.1410E-04	0.488	A1-2

Table 1. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
196	4	1	146	1926	211	-54	0.3501E-04	0.2311E-04	0.660	0.1693E-04	0.484	A1-3
197	4	2	5	1935	148	56	0.3125E-04	0.2284E-04	0.731	0.1657E-04	0.530	A1-2
198	4	2	16	1946	151	55	0.3050E-04	0.1868E-04	0.612	0.1340E-04	0.439	A1-2
199	4	2	26	1956	154	52	0.3490E-04	0.2103E-04	0.603	0.1454E-04	0.417	A1-2
200	4	2	36	1966	150	48	0.3636E-04	0.2664E-04	0.733	0.1837E-04	0.505	A1-2
201	4	2	46	1976	149	55	0.3557E-04	0.2171E-04	0.610	0.1592E-04	0.447	A1-2
202	4	2	56	1986	341	-49	0.6369E-05	0.8841E-05	1.388	0.7515E-05	1.180	A1-2
203	4	2	66	1996	324	-39	0.2436E-05	0.9928E-05	4.076	0.7875E-05	3.233	A1-2
204	4	2	76	2006	305	-58	0.6574E-05	0.1216E-04	1.850	0.1046E-04	1.591	A1-2
205	4	2	86	2016	157	47	0.2272E-04	0.1103E-04	0.486	0.6830E-05	0.301	A1-2
206	4	2	96	2026	151	54	0.2405E-04	0.1227E-04	0.510	0.8846E-05	0.368	A1-2
207	4	2	106	2036	210	-49	0.2257E-04	0.1092E-04	0.484	0.7020E-05	0.311	A1-2
208	4	2	116	2046	343	-44	0.6619E-05	0.2276E-05	0.344	0.2285E-05	0.345	A1-2
209	4	2	126	2056	334	-59	0.4080E-05	0.1040E-04	2.549	0.7921E-05	1.941	A1-2
210	4	2	136	2066	347	-54	0.5506E-05	0.3833E-05	0.696	0.3293E-05	0.598	A1-2
211	4	2	146	2076	158	47	0.1404E-04	0.2948E-05	0.210	0.2137E-05	0.152	A1-2
212	4	3	6	2086	169	45	0.3105E-04	0.1817E-04	0.585	0.1303E-04	0.420	A1-2
213	4	3	16	2096	163	51	0.2662E-04	0.1681E-04	0.631	0.1244E-04	0.467	A1-2
214	4	3	26	2106	171	48	0.3024E-04	0.1541E-04	0.510	0.1088E-04	0.360	A1-2
215	4	3	36	2116	165	54		0.1710E-04		0.1140E-04		A1-4
216	4	3	46	2126	163	52	0.3315E-04	0.2047E-04	0.617	0.1452E-04	0.438	A1-2
217	4	3	56	2136	187	61	0.1248E-04	0.5346E-05	0.428	0.3171E-05	0.254	A1-2
218	4	3	66	2146	348	-47	0.2933E-05	0.6702E-05	2.285	0.5799E-05	1.977	A1-2
219	4	3	76	2156	7	51	0.2546E-05	0.7828E-05	3.074	0.6733E-05	2.644	A1-6
220	4	3	86	2166	345	-52	0.3696E-05	0.1145E-04	3.098	0.9502E-05	2.571	A1-2
221	4	3	96	2176	354	-55	0.6523E-05	0.1544E-04	2.367	0.1260E-04	1.938	A1-5
222	4	3	106	2186	348	-57	0.5785E-05	0.1478E-04	2.555	0.1156E-04	1.998	A1-2
223	4	3	116	2196	339	-48	0.3430E-05	0.1190E-04	3.465	0.9210E-05	2.685	A1-2
224	4	3	126	2206	353	-54	0.1057E-04	0.1896E-04	1.793	0.1440E-04	1.362	A1-2
225	4	3	136	2216	338	-54	0.5295E-05	0.1374E-04	2.596	0.1036E-04	1.957	A1-2
226	4	3	146	2226	353	-55	0.1046E-04	0.1750E-04	1.673	0.1270E-04	1.214	A1-2
227	4	4	6	2236	333	-55	0.3953E-05	0.1127E-04	2.851	0.9036E-05	2.286	A1-2
228	4	4	16	2246	339	-54	0.9072E-05	0.1442E-04	1.590	0.1062E-04	1.171	A1-2
229	4	4	26	2256	343	-54	0.2693E-05	0.1048E-04	3.892	0.7503E-05	2.787	A1-2
230	4	4	36	2266	338	-56	0.5151E-05	0.1200E-04	2.329	0.9650E-05	1.873	A1-2
231	4	4	46	2276	187	54	0.1424E-04	0.4159E-05	0.292	0.2403E-05	0.169	A1-2
232	4	4	56	2286	164	57	0.1982E-04	0.6372E-05	0.322	0.4415E-05	0.223	A1-2
233	4	4	66	2296	314	-54	0.6774E-05	0.5122E-05	0.756	0.4154E-05	0.613	A1-2
234	4	4	76	2306	350	-61	0.7140E-05	0.6034E-05	0.845	0.4683E-05	0.656	A1-2
235	4	4	86	2316	339	-56	0.4620E-05	0.6371E-05	1.379	0.4772E-05	1.033	A1-2
236	4	4	96	2326	351	-59	0.5325E-05	0.1091E-04	2.048	0.9025E-05	1.695	A1-2
237	4	4	106	2336	182	50	0.1510E-04	0.3310E-05	0.220	0.2470E-05	0.164	A1-2
238	4	4	116	2346	174	57	0.2218E-04	0.1051E-04	0.474	0.7074E-05	0.319	A1-2
239	4	4	126	2356	336	-56	0.3885E-05	0.3880E-05	0.999	0.3063E-05	0.788	A1-2
240	4	4	136	2366	354	-57	0.2981E-05	0.8204E-05	2.753	0.6701E-05	2.248	A1-2
241	4	4	146	2376	308	- 4	0.2554E-05	0.1005E-04	3.935	0.7620E-05	2.983	L5
242	4	5	6	2386	355	-52	0.6994E-05	0.3390E-05	0.485	0.3337E-05	0.477	A1-2
243	4	5	16	2396	182	47	0.1863E-04	0.8131E-05	0.436	0.5263E-05	0.283	A1-2
244	4	5	26	2406	361	-44	0.6492E-05	0.7039E-05	1.084	0.5456E-05	0.840	A1-2
245	4	5	36	2416	356	-53	0.1844E-05	0.9002E-05	4.881	0.6547E-05	3.550	A1-2
246	4	5	46	2426	354	-58	0.9185E-05	0.5570E-05	0.606	0.4489E-05	0.489	A1-2
247	4	5	56	2436	177	51	0.2542E-04	0.1321E-04	0.520	0.9302E-05	0.366	A1-2
248	4	5	66	2446	175	57	0.2300E-04	0.1023E-04	0.445	0.7020E-05	0.305	A1-2
249	4	5	76	2456	174	52	0.1862E-04	0.8785E-05	0.472	0.5941E-05	0.319	A1-2
250	4	5	86	2466	185	52	0.2713E-04	0.1023E-04	0.377	0.6835E-05	0.252	A1-2
251	4	5	96	2476	338	-68	0.7109E-05	0.3792E-05	0.533	0.2859E-05	0.402	A1-2
252	4	5	106	2486	304	- 3	0.5865E-05	0.4772E-05	0.814	0.3833E-05	0.654	A1-2
253	4	5	116	2496	5	-53	0.6473E-05	0.3784E-05	0.585	0.2994E-05	0.462	A1-2
254	4	5	126	2506	3	-52	0.5017E-05	0.1350E-04	2.692	0.9285E-05	1.851	A1-2
255	4	5	136	2516	3	-54	0.4274E-05	0.1013E-04	2.370	0.8197E-05	1.918	A1-2

Table 1. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
256	4	5	146	2526	360	-52	0.6473E-05	0.8143E-05	1.258	0.7055E-05	1.090	A1-2
257	4	6	6	2536	341	-53	0.4195E-05	0.8681E-05	2.070	0.6251E-05	1.490	A1-2
258	4	6	16	2546	349	-53	0.7811E-05	0.1071E-04	1.371	0.8373E-05	1.072	A1-3
259	4	6	26	2556	351	-50	0.3809E-05	0.1025E-04	2.692	0.7322E-05	1.922	A1-2
260	4	6	36	2566	350	-48	0.7718E-05	0.1255E-04	1.626	0.9998E-05	1.295	A1-2
261	4	6	46	2576	333	-21	0.1197E-04	0.9133E-05	0.763	0.6255E-05	0.523	A1-2
262	4	6	56	2586	353	-45	0.1070E-04	0.1026E-04	0.959	0.7739E-05	0.723	A1-3
263	4	6	66	2596	333	-30	0.1940E-04	0.4439E-05	0.229	0.3402E-05	0.175	A1-3
264	4	6	76	2606	340	-20	0.2007E-04	0.7299E-05	0.364	0.5903E-05	0.294	A1-4
265	4	6	86	2616	9	-66	0.1018E-04	0.1165E-04	1.145	0.1042E-04	1.024	A1-4
266	4	6	96	2626	335	-45	0.2680E-04	0.4657E-05	0.174	0.3894E-05	0.145	A1-3
267	4	6	106	2636	286	-38	0.2784E-04	0.1506E-05	0.054	0.1220E-05	0.044	A2-3
268	4	6	116	2646	21	-13	0.2460E-04	0.5160E-05	0.210	0.3871E-05	0.157	A1-4
269	4	6	126	2656	294	-24	0.8764E-06	0.3429E-06	0.391	0.2684E-06	0.306	L3
270	4	6	136	2666	281	-10	0.3355E-04	0.1105E-05	0.033	0.1019E-05	0.030	L3
271	4	6	146	2676	309	-48	0.2471E-05	0.1155E-06	0.047	0.1431E-06	0.058	L3
272	4	7	6	2686	282	- 7	0.3009E-04	0.4030E-05	0.134	0.2337E-05	0.078	L3
273	4	7	16	2696	265	-20	0.1983E-05	0.3099E-06	0.156	0.2335E-06	0.118	A1-3
274	4	7	26	2706	357	-40	0.2575E-04	0.1507E-05	0.059	0.1591E-05	0.062	L3
275	4	7	36	2716	275	-14	0.1873E-05	0.2403E-06	0.128	0.9944E-07	0.053	L2.5
276	4	7	46	2726	77	17		0.2343E-05		0.2260E-05		A2-4
277	5	1	36				0.2222E-04	0.1094E-04	0.492	0.7064E-05	0.318	F
278	5	1	46	2866	148	-78	0.9231E-05	0.8187E-05	0.887	0.6140E-05	0.665	A1-4
279	5	1	56	2876	243	-66	0.7358E-05	0.1463E-04	1.988	0.9413E-05	1.279	A1-2
280	5	1	66	2886	220	-69	0.1049E-04	0.1135E-04	1.082	0.7999E-05	0.763	A1-3
281	5	1	76	2896	225	-71	0.5771E-05	0.1108E-04	1.919	0.3188E-04	5.525	A1-3
282	5	1	86	2906	233	-78	0.8572E-05	0.8915E-05	1.040	0.6218E-05	0.725	A1-3
283	5	1	96	2916	228	-64	0.8385E-05	0.9506E-05	1.134	0.6085E-05	0.726	A1-2
284	5	1	106	2926	64	13	0.1837E-04	0.4820E-05	0.262	0.3260E-05	0.178	A1-3
285	5	1	116	2936	71	6	0.1356E-04	0.4475E-05	0.330	0.2375E-05	0.175	A1-4
286	5	1	126	2946	95	-37	0.1402E-04	0.2451E-05	0.175	0.1442E-05	0.103	A1.5-3
287	5	1	136	2956	87	- 4	0.1056E-04	0.2350E-05	0.223	0.1409E-05	0.133	A1-4
288	5	1	146	2966	48	3	0.1463E-04	0.3212E-05	0.220	0.2140E-05	0.146	A1-3
289	5	2	56				0.4445E-05	0.5173E-05	1.164	0.3192E-05	0.718	F
290	5	2	116				0.8428E-05	0.5912E-05	0.701	0.3551E-05	0.421	F
291	5	3	23				0.3968E-05	0.3047E-05	0.768	0.1970E-05	0.496	F
292	5	3	99				0.1196E-04	0.4016E-05	0.336	0.2296E-05	0.192	F
293	5	4	76				0.4096E-05	0.5938E-05	1.450	0.4248E-05	1.037	F
294	5	5	46				0.1002E-04	0.1023E-04	1.021	0.7204E-05	0.719	F
295	5	5	56	3166	230	-45	0.1377E-04	0.1717E-05	0.125	0.1124E-05	0.082	L2
296	5	5	66	3176	321	45	0.1507E-04	0.1925E-05	0.128	0.6429E-06	0.043	A1-2
297	5	5	76	3186	305	-50	0.1102E-04	0.9520E-06	0.086	0.4319E-06	0.039	L2
298	5	5	86	3196	352	-53	0.2570E-04	0.3604E-05	0.140	0.1510E-05	0.059	L2
299	5	5	96	3206	360	52	0.2001E-04	0.5148E-05	0.257	0.3276E-05	0.164	A1-2
300	5	5	106	3216	316	-38	0.1751E-04	0.1240E-05	0.071	0.4285E-06	0.024	L2
301	5	5	119	3229	352	43	0.3900E-04	0.4930E-05	0.126	0.2595E-05	0.067	A1-2
302	5	5	130	3240	308	- 5	0.2796E-04	0.9760E-05	0.349	0.5360E-05	0.192	A1-4
303	5	5	146	3256	4	50	0.4197E-04	0.9771E-05	0.233	0.6490E-05	0.155	A1-2
304	5	6	6	3266	330	55	0.2569E-04	0.5202E-05	0.202	0.3078E-05	0.120	A1-2
305	5	6	16	3276	287	4	0.2975E-04	0.3134E-05	0.105	0.2204E-05	0.074	L3
306	5	6	26	3286	255	14	0.2359E-04	0.3432E-05	0.145	0.2357E-05	0.100	L3
307	5	6	36	3296	352	48	0.3866E-04	0.8010E-05	0.207	0.4833E-05	0.125	A1-2
308	5	6	46	3306	305	30	0.2188E-04	0.4753E-05	0.217	0.2879E-05	0.132	L2
309	5	6	56	3316	315	-14	0.2352E-04	0.3845E-05	0.163	0.2694E-05	0.115	A3-4
310	5	6	66	3326	336	36	0.1820E-04	0.4230E-05	0.230	0.2320E-05	0.127	A1-2
311	5	6	76	3336	294	-22	0.2021E-04	0.2613E-05	0.129	0.2189E-05	0.108	L3
312	5	6	86	3346	293	- 9	0.1467E-04	0.1967E-05	0.134	0.1028E-05	0.070	L3
313	5	6	96	3356	301	26	0.2851E-04	0.3488E-05	0.122	0.1993E-05	0.070	L3
314	5	6	107	3367	265	- 9	0.1136E-04	0.1953E-05	0.172	0.1395E-05	0.123	A3-4
315	5	6	116	3376	303	21	0.2381E-04	0.3597E-05	0.151	0.2165E-05	0.091	L3

Table 1. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
316	5	6	126	3386	346	18	0.1622E-04	0.3762E-05	0.232	0.2371E-05	0.146	A2-3
317	5	6	135	3395	339	39	0.2411E-04	0.5267E-05	0.218	0.3423E-05	0.142	L2
318	5	7	145	3405	325	38	0.1594E-04	0.4964E-05	0.311	0.2478E-05	0.155	L2
319	5	7	6	3416	305	31	0.1947E-04	0.2338E-05	0.120	0.1538E-05	0.079	L2
320	5	7	16	3426	345	39	0.1970E-04	0.3460E-05	0.176	0.1680E-05	0.085	L2
321	5	7	26	3436	296	- 6	0.2181E-04	0.2481E-05	0.114	0.2162E-05	0.099	L2
322	5	7	36	3446	342	55	0.2310E-04	0.3881E-05	0.168	0.1804E-05	0.078	A1-2
323	5	7	45	3455	295	37	0.2354E-04	0.1720E-05	0.073	0.1031E-05	0.044	A1-2
324	6	1	131				0.3565E-04	0.3462E-04	0.971	0.2303E-04	0.646	F
325	6	1	141				0.6250E-04	0.3430E-04	0.549	0.2305E-04	0.369	F
326	6	2	121				0.3568E-04	0.1145E-04	0.321	0.6468E-05	0.181	F
327	6	2	131				0.4555E-04	0.7762E-05	0.170	0.4799E-05	0.105	F
328	6	2	141				0.2656E-04	0.8816E-05	0.332	0.6023E-05	0.227	F
329	6	3	6				0.4077E-04	0.9182E-05	0.225	0.5860E-05	0.144	F
330	6	3	26				0.1941E-04	0.9594E-05	0.494	0.6622E-05	0.341	F
331	6	3	16				0.4196E-04	0.1013E-04	0.241	0.6475E-05	0.154	F
332	6	3	36				0.2396E-04	0.9235E-05	0.385	0.5967E-05	0.249	F
333	6	3	46				0.1408E-04	0.8356E-05	0.594	0.5899E-05	0.419	F
334	6	3	56				0.2239E-04	0.1019E-04	0.455	0.6452E-05	0.288	F
335	6	3	66				0.3231E-04	0.9009E-05	0.279	0.5245E-05	0.162	F
336	6	3	76	3516	121	47	0.2965E-04	0.9127E-05	0.308	0.5950E-05	0.201	A1-2
337	6	3	86	3526	215	-54	0.2608E-04	0.8938E-05	0.343	0.6089E-05	0.233	A1-2
338	6	3	96	3536	139	58	0.3078E-04	0.9072E-05	0.295	0.7191E-05	0.234	A1-2
339	6	3	106	3546	135	59	0.3198E-04	0.9718E-05	0.304	0.5934E-05	0.186	A1-2
340	6	3	116	3556	260	-47	0.2477E-04	0.2257E-05	0.090	0.2091E-05	0.080	A1-4
341	6	3	126	3566	129	37	0.4301E-04	0.7775E-05	0.181	0.4456E-05	0.104	A1-2
342	6	3	136	3576	164	29	0.2916E-04	0.8587E-05	0.294	0.5498E-05	0.189	A1-4
343	6	3	146	3586	205	-37	0.2061E-04					L4
344	6	4	6	3596	210	-34	0.1946E-04	0.8571E-05	0.440	0.6303E-05	0.324	A1-3
345	6	4	16	3606	219	-56	0.1685E-04					A4-5
346	6	4	26	3616	212	-52	0.2229E-04	0.2921E-05	0.131	0.2902E-05	0.130	L2
347	6	4	36	3626	46	8	0.4372E-04					A5-8
348	6	4	46	3636	65	45	0.4285E-04	0.1491E-04	0.348	0.1045E-04	0.244	A1-2
349	6	4	56	3646	106	13	0.5334E-04					L6
350	6	4	66	3656	44	50	0.2894E-04	0.6069E-05	0.210	0.3759E-05	0.130	A1-3
351	6	4	76	3666	47	49	0.2629E-04			0.6424E-05	0.244	A1-2
352	6	4	86	3676	72	52	0.1697E-04	0.4195E-05	0.247	0.3609E-05	0.213	A1-3
353	6	4	96	3686	50	11	0.2631E-04			0.2778E-05	0.106	A4-6
354	6	4	106	3696	223	-65	0.1374E-04	0.3249E-05	0.236	0.3811E-05	0.277	A1-2
355	6	4	116	3706	245	-50	0.2596E-04	0.1581E-05	0.061	0.1215E-05	0.047	L2
356	6	4	126	3716	54	20	0.3331E-04	0.1284E-04	0.385	0.5776E-05	0.173	A1-2
357	6	4	136	3726			0.2235E-04	0.7593E-05	0.340	0.3136E-05	0.140	U
358	6	4	146	3736	86	32	0.3487E-04	0.1454E-04	0.417	0.6639E-05	0.190	A1-2
359	6	5	6	3746	81	40	0.3313E-04	0.1510E-04	0.456	0.8913E-05	0.269	A1-2
360	6	5	16	3756	91	47	0.2421E-04	0.1288E-04	0.532	0.7700E-05	0.318	A1-2
361	6	5	26	3766	111	60	0.1194E-04	0.9041E-05	0.757	0.6631E-05	0.555	A1-2
362	6	5	36	3776	96	41	0.2617E-04	0.1176E-04	0.449	0.7313E-05	0.279	A1-2
363	6	5	46	3786	93	57	0.1470E-04	0.6693E-05	0.455	0.4401E-05	0.299	A1-2
364	6	5	56	3796	73	64	0.1527E-04	0.8660E-05	0.567	0.5476E-05	0.359	A1-2
365	6	5	66	3806	88	62	0.1876E-04	0.8318E-05	0.443	0.5693E-05	0.303	A1-2
366	6	5	76	3816	83	45	0.1874E-04	0.3066E-05	0.164	0.2315E-05	0.123	A1-2
367	6	5	86	3826	90	36	0.1490E-04	0.1050E-04	0.704	0.7100E-05	0.476	A1-2
368	6	5	96	3836	109	14	0.1858E-04	0.3941E-05	0.212	0.2326E-05	0.125	A1-2
369	6	5	106	3846	116	36	0.1315E-04	0.5332E-05	0.406	0.3974E-05	0.302	A1-2
370	6	5	116	3856	121	51	0.1423E-04	0.7534E-05	0.529	0.5212E-05	0.366	A1-2
371	6	5	126	3866	123	44	0.1203E-04	0.6856E-05	0.570	0.4613E-05	0.384	A1-2
372	6	5	136	3876	142	34	0.2162E-04	0.4798E-05	0.222	0.2556E-05	0.118	A1-2
373	6	5	146	3886	125	-13	0.2207E-04	0.9216E-05	0.418	0.1544E-05	0.070	L3
374	6	6	6	3896	183	-43	0.2958E-04	0.1074E-04	0.363	0.4622E-05	0.156	A1-2
375	6	6	16	3906	211	-68	0.1659E-04	0.6864E-05	0.414	0.2950E-05	0.178	A1-2

Table 1. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
376	6	6	26	3916			0.1122E-04			0.2300E-05	0.205	U
377	6	6	36	3926	183	33	0.1956E-04	0.5581E-05	0.285	0.2387E-05	0.122	L3
378	6	6	46	3936	216	-43	0.3572E-04			0.1265E-04	0.354	A2-3
379	6	6	56	3946	52	34	0.1379E-04	0.3150E-05	0.228	0.3120E-05	0.226	A1-2
380	6	6	66	3956	42	61	0.2211E-04	0.7257E-05	0.328	0.4665E-05	0.211	A1-2
381	6	6	76	3966	245	-32	0.1268E-04	0.2535E-05	0.200	0.3233E-05	0.255	L2
382	6	6	86	3976	31	46	0.3564E-04	0.1418E-04	0.398	0.5887E-05	0.165	A1-2
383	6	6	96	3986	299	48	0.2244E-04	0.4701E-05	0.209	0.1306E-05	0.058	L2
384	6	6	106	3996	290	27	0.3123E-04	0.9583E-05	0.307	0.3512E-05	0.112	L3
385	6	6	116	4006	30	11	0.3396E-04	0.1887E-04	0.556	0.1142E-04	0.336	L2
386	6	6	126	4016	230	-39	0.1473E-04	0.2056E-04	1.396	0.1435E-04	0.975	A1-2
387	6	6	136	4026	203	-29	0.1920E-04	0.1439E-04	0.744	0.1043E-04	0.540	A1-2
388	6	6	146	4036	3	15	0.2742E-04	0.9641E-05	0.352	0.4577E-05	0.167	A1-3
389	6	6	6	4046	255	12	0.2650E-04	0.3628E-05	0.137	0.3440E-05	0.130	L2
390	6	7	16	4056	347	25	0.2430E-04	0.9680E-05	0.405	0.7570E-05	0.311	A1-2
391	6	7	26	4066	306	27	0.2366E-04	0.7786E-05	0.329	0.6185E-05	0.261	A2-4
392	6	7	36	4076	347	34	0.3143E-04	0.1367E-04	0.435	0.9233E-05	0.294	A2-4
393	6	7	44	4084	324	38	0.3131E-04	0.9476E-05	0.303	0.7151E-05	0.228	A2-4
394	7	1	9	4469			0.8808E-05	0.1392E-04	1.580	0.9591E-05	1.089	U
395	7	1	16	4476	295	-39	0.2573E-04	0.2447E-04	0.951	0.1837E-04	0.714	A4-5
396	7	1	26	4486	357	-52	0.8892E-04	0.7187E-04	0.808	0.4567E-04	0.514	A5-6
397	7	1	36	4496	167	-61	0.1068E-03	0.8434E-04	0.789	0.5411E-04	0.506	A5-6
398	7	1	46	4506	211	-45	0.2037E-03	0.1447E-03	0.711	0.9858E-04	0.484	A5-6
399	7	1	56	4516	93	-44	0.3678E-04	0.4122E-04	1.121	0.2398E-04	0.652	A1-2
400	7	1	66	4526	130	-25	0.4627E-04	0.4419E-04	0.955	0.2555E-04	0.552	L3
401	7	1	76	4536	280	44	0.3339E-04	0.1212E-04	0.363	0.7511E-05	0.225	A1-2
402	7	1	86	4546	274	39	0.4174E-04	0.1323E-04	0.317	0.6274E-05	0.150	A1-2
403	7	1	96	4556	270	-49	0.1960E-04	0.3944E-05	0.201	0.2179E-05	0.111	L2
404	7	1	106	4566	302	14	0.4700E-04	0.2210E-04	0.470	0.1286E-04	0.274	A1-2
405	7	1	116	4576	137	-20	0.1791E-04	0.9119E-05	0.509	0.6864E-05	0.383	L3
406	7	1	126	4586	261	28	0.3095E-04	0.7115E-05	0.230	0.2435E-05	0.079	A1-2
407	7	1	136	4596	101	-28	0.2165E-04	0.1298E-05	0.060	0.2576E-05	0.119	A1-2
408	7	1	146	4606	283	1	0.2701E-04			0.1100E-04	0.407	A2-5
409	7	2	5				0.6749E-05	0.1857E-04	2.752	0.1284E-04	1.903	F
410	7	2	26				0.2066E-04					F
411	7	2	36				0.1528E-04			0.9085E-06	0.059	F
412	7	2	56	4616	98	-26	0.2455E-04	0.3002E-04	1.223	0.1400E-04	0.570	A1-2
413	7	2	66	4626	118	-25	0.2412E-04	0.3141E-04	1.302	0.1570E-04	0.651	A1-2
414	7	2	76	4636	119	-19	0.5188E-04	0.4247E-04	0.819	0.2067E-04	0.398	A1-2
415	7	2	86	4646	114	-25	0.4050E-04	0.4293E-04	1.060	0.1960E-04	0.484	A1-3
416	7	2	96	4656	111	-38	0.3891E-04	0.5095E-04	1.310	0.2686E-04	0.690	A1-2
417	7	2	108	4666	272	57	0.3520E-04	0.1056E-04	0.300	0.4709E-05	0.134	A1-2
418	7	2	116	4676	290	33	0.7185E-04	0.3360E-04	0.468	0.1624E-04	0.226	A1-2
419	7	2	126	4686	253	35	0.3001E-04	0.6461E-05	0.215	0.2698E-05	0.090	A1-2
420	7	2	136	4696	272	36	0.8055E-04	0.3507E-04	0.435	0.1888E-04	0.234	A1-2
421	7	2	146	4706	279	20	0.4221E-04	0.1507E-04	0.357	0.8146E-05	0.193	L4
422	7	3	5	4716	258	23	0.3232E-04	0.4115E-05	0.127	0.1594E-05	0.049	L3
423	7	3	14	4726	116	-32	0.1249E-04	0.1113E-04	0.891	0.6438E-05	0.515	A1-2
424	7	3	26	4736	242	12	0.3523E-04	0.3187E-05	0.090	0.2027E-05	0.058	A2-4
425	7	3	36	4746	159	-23	0.1756E-04	0.5638E-05	0.321	0.3156E-05	0.180	A4-5
426	7	3	46	4756	223	-18	0.2423E-04	0.2587E-05	0.107	0.1738E-05	0.072	A4-5
427	7	3	56	4766	286	-23	0.1939E-04	0.2133E-05	0.110			L5
428	7	3	66	4776	109	-38	0.9600E-05	0.2186E-04	2.277	0.1527E-04	1.590	L2
429	7	3	76	4786	272	25	0.2820E-04	0.3801E-05	0.135	0.1908E-05	0.068	A2-4
430	7	3	86	4796	89	-33	0.2947E-04	0.8012E-05	0.272	0.4910E-05	0.167	A1-2
431	7	3	96	4806	99	-46	0.2420E-04	0.1178E-04	0.487	0.8743E-05	0.361	L2
432	7	3	106	4816	305	-40	0.2269E-04	0.6747E-05	0.297	0.6384E-05	0.281	A3-5
433	7	3	116	4826	280	32	0.4513E-04	0.1747E-04	0.387	0.1185E-04	0.263	A1-2
434	7	3	126	4836	283	31	0.7154E-04	0.2876E-04	0.402	0.1846E-04	0.258	A1-3
435	7	3	136	4846	277	34	0.6464E-04	0.2780E-04	0.430	0.1811E-04	0.280	A1-2

Table 1. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
436	7	3	146	4856	275	36	0.7666E-04	0.2546E-04	0.332	0.1650E-04	0.215	A1-3
437	7	4	6	4866	272	30	0.7949E-04	0.4434E-04	0.558	0.2997E-04	0.377	A1-2
438	7	4	16	4876	266	34	0.8817E-04	0.3812E-04	0.432	0.2467E-04	0.280	A1-3
439	7	4	26	4886	263	42	0.4568E-04	0.1264E-04	0.277	0.6944E-05	0.152	A1-2
440	7	4	36	4896	278	40	0.4744E-04	0.3458E-05	0.073	0.1792E-05	0.038	A1-3
441	7	4	46	4906	270	36	0.3890E-04	0.6610E-05	0.170	0.4413E-05	0.113	A1-2
442	7	4	56	4916	251	49	0.3745E-04	0.3025E-05	0.081	0.1678E-05	0.045	L3
443	7	4	66	4926	242	46	0.3315E-04	0.5658E-05	0.171	0.3795E-05	0.114	A1-2
444	7	4	76	4936	114	-24	0.3124E-04	0.1617E-04	0.518	0.9588E-05	0.307	A1-3
445	7	4	86	4946	231	39	0.3617E-04	0.2662E-05	0.074	0.2148E-05	0.059	A1-2
446	7	4	96	4956	61	-25	0.2977E-04	0.5545E-05	0.186	0.4708E-05	0.158	A2-3
447	7	4	106	4966	71	-26	0.2411E-04	0.8078E-05	0.335	0.6789E-05	0.282	L3
448	7	4	116	4976	238	26	0.4212E-04	0.5385E-05	0.128	0.2747E-05	0.065	A1-2
449	7	4	126	4986	265	42	0.3993E-04	0.7597E-05	0.190	0.4415E-05	0.111	A1-2
450	7	4	136	4996	62	17	0.3510E-04	0.5517E-05	0.157	0.3309E-05	0.094	A1-2
451	7	4	146	5006	91	-36	0.3113E-04	0.1585E-04	0.509	0.9317E-05	0.299	L3
452	7	5	6	5016	76	- 6	0.1980E-04	0.1011E-04	0.510	0.5986E-05	0.302	A1-2
453	7	5	16	5026	115	-16	0.2974E-04	0.4024E-05	0.135	0.3274E-05	0.110	A2-3
454	7	5	26	5036	274	40	0.3521E-04	0.7357E-05	0.209	0.4495E-05	0.128	A1-2
455	7	5	36	5046	260	51	0.4453E-04	0.1006E-04	0.226	0.7554E-05	0.170	A1-2
456	7	5	46	5056	255	24	0.5667E-04	0.2457E-04	0.434	0.1618E-04	0.286	A1-2
457	7	5	56	5066	267	48	0.4358E-04	0.1309E-04	0.300	0.9436E-05	0.216	A1-2
458	7	5	66	5076	272	62	0.3938E-04	0.6974E-05	0.177	0.4282E-05	0.109	A1-2
459	7	5	76	5086	229	27	0.3146E-04	0.4568E-05	0.145	0.3060E-05	0.097	A3-4
460	7	5	86	5096	242	34	0.3861E-04	0.6251E-05	0.162	0.3807E-05	0.099	L3
461	7	5	96	5106	238	46	0.1746E-04	0.5472E-05	0.313	0.3847E-05	0.220	A3-4
462	7	5	106	5116	76	-40	0.2549E-04	0.5681E-05	0.223	0.3550E-05	0.139	A1-2
463	7	5	116	5126	250	55	0.2939E-04	0.6566E-05	0.223	0.4987E-05	0.170	A1-2
464	7	5	126	5136	238	48	0.4695E-04	0.7424E-05	0.158	0.4708E-05	0.100	A1-2
465	7	5	136	5146	79	-18	0.1764E-04	0.1472E-04	0.834	0.9101E-05	0.516	L3
466	7	5	146	5156	100	-40	0.2715E-04	0.9809E-05	0.361	0.4623E-05	0.170	L2
467	7	6	6	5166	258	70	0.4191E-04	0.5377E-05	0.128	0.3572E-05	0.085	A1-2
468	7	6	16	5176	216	64	0.3050E-04	0.3661E-05	0.120	0.2663E-05	0.087	L2
469	7	6	26	5186	119	-17	0.3454E-04	0.7383E-05	0.214	0.3726E-05	0.108	L3
470	7	6	36	5196	268	55	0.3569E-04	0.6023E-05	0.169	0.5321E-05	0.149	L2
471	7	6	46	5206	102	8	0.3202E-04	0.4401E-05	0.137	0.2805E-05	0.088	A1-2.5
472	7	6	56	5216	94	-28	0.2095E-04	0.1016E-04	0.485	0.7101E-05	0.339	L3
473	7	6	66	5226	296	42	0.3216E-04	0.5130E-05	0.159	0.1616E-05	0.050	A1-2
474	7	6	76	5236	83	26	0.3417E-04	0.2891E-05	0.085	0.1348E-05	0.039	L2
475	7	6	86	5246			0.3473E-04	0.2459E-05	0.071	0.1863E-05	0.054	U
476	7	6	96	5256	242	45	0.3718E-04	0.5498E-05	0.148	0.2318E-05	0.062	A1-2
477	7	6	106	5266	283	35	0.4264E-04	0.9500E-05	0.220	0.4776E-05	0.112	A2-4
478	7	6	116	5276	284	33	0.4412E-04	0.1057E-04	0.240	0.6171E-05	0.140	A1-2
479	7	6	126	5286	48	-19	0.3240E-04	0.6910E-05	0.213	0.3890E-05	0.120	L3
480	7	6	136	5296	94	-29	0.2153E-04	0.1346E-04	0.625	0.9467E-05	0.440	L3
481	7	6	146	5306	108	-15	0.3452E-04	0.2821E-04	0.817	0.2102E-04	0.609	A1-4
482	7	7	6	5316	100	-21	0.2115E-04	0.1512E-04	0.715	0.1201E-04	0.568	L2
483	7	7	16	5326	127	-26	0.3797E-04	0.3838E-05	0.101	0.4624E-05	0.122	L2
484	7	7	26	5336	293	51	0.4167E-04	0.4277E-05	0.103	0.1615E-05	0.039	L1
485	7	7	36	5346	259	45	0.3958E-04	0.6848E-05	0.173	0.3565E-05	0.090	A2-3
486	7	7	46	5356	37	-35	0.3210E-04	0.2581E-05	0.080	0.2309E-05	0.072	L2
487	8	1	26	5436	146	-51	0.2103E-04	0.2761E-04	1.313	0.1900E-04	0.904	L5
488	8	1	36	5446	118	-67	0.3259E-04	0.1314E-04	0.403	0.9773E-05	0.300	A1-5
489	8	1	46	5456	143	-18	0.7447E-04	0.3549E-04	0.477	0.2502E-04	0.336	L5
490	8	1	56	5466	318	-53	0.2850E-04	0.1308E-04	0.459	0.1030E-04	0.361	A1-5
491	8	1	66	5476	312	-41	0.3130E-04			0.1094E-04	0.349	A1-3
492	8	1	76	5486	319	-40	0.4522E-04	0.2089E-04	0.462	0.1554E-04	0.344	A1-2
493	8	1	86	5496	327	-45	0.3797E-04	0.1550E-04	0.408	0.1266E-04	0.334	A1-2
494	8	1	96	5506	190	1	0.8664E-04	0.1168E-04	0.135	0.5045E-05	0.058	L2
495	8	1	106	5516	327	-13	0.3277E-04	0.2405E-04	0.734	0.1807E-04	0.552	A1-3

Table 1. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
496	8	1	116	5526	328	-34	0.4651E-04	0.2001E-04	0.430	0.1615E-04	0.347	A1-2
497	8	1	126	5536	340	-18	0.1956E-04	0.3853E-04	1.969	0.2857E-04	1.460	A1-2
498	8	1	136	5546	190	- 3	0.6552E-04	0.1249E-04	0.191	0.8773E-05	0.134	A1-3
499	8	1	146	5556	321	-20	0.2987E-04	0.2493E-04	0.835	0.1628E-04	0.545	A1-3
500	8	2	5	5565	137	15	0.9755E-04	0.4520E-04	0.463	0.3423E-04	0.351	A1-4
501	8	2	22	5582	319	-12	0.3062E-04	0.1543E-04	0.504	0.1151E-04	0.376	A1-2
502	8	2	32	5592	141	17	0.7556E-04	0.2639E-04	0.349	0.2145E-04	0.284	A1-4
503	8	2	67	5627	178	49	0.4953E-04	0.5108E-05	0.103	0.3312E-05	0.067	A1-3
504	8	2	78	5638	312	-35	0.3043E-04	0.1294E-04	0.425	0.8765E-05	0.288	A1-2
505	8	2	106	5666	140	19	0.7197E-04	0.2976E-04	0.413	0.2353E-04	0.327	A1-3
506	8	2	116	5676	317	-19	0.1928E-04	0.3857E-04	2.000	0.2609E-04	1.353	A1-2
507	8	2	126	5686	292	- 9	0.5458E-04	0.5365E-05	0.098	0.3738E-05	0.068	L3
508	8	2	136	5696	313	-17	0.3127E-04	0.5674E-04	1.814	0.3803E-04	1.216	A1-2
509	8	2	146	5706	304	54	0.3881E-04	0.3727E-05	0.096	0.2555E-05	0.066	L2
510	8	3	4	5714	132	21	0.6602E-04	0.2373E-04	0.360	0.1600E-04	0.242	A1-2
511	8	3	66	5776	123	-20	0.3812E-04	0.6045E-05	0.159	0.2732E-05	0.072	L3
512	8	3	92	5802	249	-27	0.5272E-04	0.9811E-05	0.186	0.4145E-05	0.079	A1-2
513	8	3	101	5811	146	18	0.5164E-04			0.3351E-05	0.065	A2.5-3
514	8	3	147	5857	311	-14	0.3123E-04	0.1034E-04	0.331	0.9479E-05	0.304	L1
515	8	4	3	5863	132	-18	0.1948E-04	0.1337E-04	0.686	0.1121E-04	0.576	L2
516	8	4	13	5873	318	27	0.5460E-04	0.2600E-04	0.476	0.1740E-04	0.318	A1-2
517	8	4	23	5883	114	9	0.2491E-04	0.9294E-05	0.373	0.5722E-05	0.230	L4
519	8	5	84	6094			0.78160-05	0.5142E-05	0.658	0.3232E-05	0.414	U
521	8	6	77	6237				0.5670E-04		0.4068E-04		U
522	8	6	90	6250	345	-14	0.3189E-04	0.4845E-04	1.519	0.3403E-04	1.067	A1-4
523	8	7	39	6349	157	-12	0.2280E-04	0.2657E-05	0.117	0.2048E-05	0.090	A2-3
524	8	*	6	6359	328	- 6	0.3526E-04	0.7382E-05	0.209	0.6771E-05	0.192	L2

Note: A = vector average of declination and inclination values at demagnetization levels (x 100) shown.
L = demagnetization level (x 100) used to define declination and inclination. U = magnetically unstable sample.
F = flow-in material (based on shipboard visual descriptions).

variable values below about 45 m. In contrast, J_{100} values tend to decrease downcore, but again with a marked increase in variance below about 45 m. The J_{100}/J_0 ratio (Fig. 4) emphasizes the contrast, with a major trend from values near 1 above about 18 m to close to zero below about 29 m. Demagnetization curves above (Fig. 5A, B, C) and below (Fig. 5D, E, F) the lithologic change illustrate the marked change in magnetic properties. The shallower samples show a steady decrease in intensity with increasing AF strength, with little change in the direction of magnetization. Even at 400 Oe, J_{400}/J_0 values exceed 0.25. In contrast, the deeper samples show marked intensity changes (Fig. 5D) or a rapid J/J_0 decrease to values of 0.1 or less at AF strengths of 100 Oe or more (Fig. 5E, F).

The coincidence of the transitional change in lithology, loss of paleomagnetic stratigraphy, and decrease in J_{100} (both absolute and relative to NRM) point to a common sedimentological cause for these phenomena.

Site 578

Site 578 yielded an excellent magnetic record (Tables 6 and 7). Even on the *Challenger*, it was clear that all the magnetic events in the first four chrons were present (see Site 578 chapter, this volume; Fig. 6). Subsequent shore-based laboratory studies suggest that, with the exception of a 600,000-yr. hiatus from 8.2 to 8.8 m.y. ago, all reversals from 15 m.y. ago to the present were recovered (Table 8). In the complex interval from the base of the Gilbert Epoch to Anomaly 5B (Fig. 7), only five samples from Site 578 (indicated by asterisks in Table 8) do not fit the standard stratigraphy.

The sequence of 60 identifiable reversals yields an extremely detailed age-depth curve (Fig. 8), the upper part of which is generally similar in form to the Site 576 curve (Fig. 2).

As at Site 576, the reversal stratigraphy is based primarily on inclination data. The declinations support these picks, but the absolute values are unknown and rotations within a single HPC can exceed 120° (Fig. 9). The depth at which the reversal stratigraphy breaks down (~145 m) again corresponds to the level at which the sedimentation rate drops below about 2 m/m.y. At Site 578, this level lies well within a dark brown unit that is magnetically uninterpretable at Site 576, suggesting that sedimentation rate has a greater influence on the stability of detrital remanence than does gross lithology. The brown to dark brown boundary at about 125 m marks the point at which the sedimentation rate drops below about 4 m/m.y., but the detrital sedimentation rate was

Table 2. Magnetic properties of samples from Hole 576B.

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
551	1	1	6	6	230	44	0.2352E-04	0.2050E-04	0.872	0.1564E-04	0.665	L1-2
553	1	1	26	26	231	49	0.3669E-04	0.3131E-04	0.853	0.2903E-04	0.791	L1-2
555	1	1	46	46	234	43	0.3506E-04	0.2647E-04	0.755	0.2207E-04	0.630	L1-2
557	1	1	66	66	230	51	0.3593E-04	0.3210E-04	0.893	0.2375E-04	0.661	L1-2
559	1	1	86	86	254	57	0.3930E-04	0.3476E-04	0.884	0.3009E-04	0.766	L1-2
561	1	1	106	106	260	62	0.3764E-04	0.3352E-04	0.891	0.2432E-04	0.646	L1-2
563	1	1	126	126	228	49	0.2240E-04	0.1724E-04	0.770	0.1362E-04	0.608	L1-2
565	1	2	146	146	265	50	0.3510E-04	0.2973E-04	0.847	0.2397E-04	0.683	L1-2
567	1	2	16	166	272	47	0.3218E-04	0.2940E-04	0.913	0.2502E-04	0.778	L1-2
569	1	2	36	186	267	49	0.2631E-04	0.2488E-04	0.946	0.1917E-04	0.729	L1-2
571	1	2	56	206	260	54	0.3129E-04	0.2721E-04	0.870	0.2439E-04	0.780	L1-2
573	1	2	76	226	270	45	0.2212E-04	0.2129E-04	0.962	0.1625E-04	0.735	L1-2
575	1	2	116	266	274	58	0.3380E-04	0.2795E-04	0.827	0.2424E-04	0.717	L1-2
577	1	2	96	246	269	58	0.2500E-04	0.2136E-04	0.854	0.1889E-04	0.755	L1-2
579	1	2	136	286	256	60	0.2554E-04	0.2104E-04	0.824	0.1585E-04	0.621	L1-2
581	1	3	6	306	278	60	0.2005E-04	0.1854E-04	0.924	0.1460E-04	0.728	L1-2
583	1	3	26	326	293	62	0.7175E-05	0.5257E-05	0.733	0.4895E-05	0.682	L1-2
585	1	3	47	347	262	41	0.3212E-04	0.2195E-04	0.684	0.1716E-04	0.534	L1-2
587	1	3	66	366	248	44	0.2489E-04	0.2149E-04	0.863	0.1796E-04	0.722	L1-2
589	1	3	86	386	240	39	0.1582E-04	0.1328E-04	0.839	0.1101E-04	0.696	L1-2
591	1	3	106	406	274	74	0.1839E-04	0.1492E-04	0.812	0.1302E-04	0.708	L1-2
593	1	3	126	426	233	59	0.2469E-04	0.1791E-04	0.726	0.1486E-04	0.602	L1-2
595	1	3	146	446	225	55	0.2510E-04	0.2241E-04	0.893	0.1856E-04	0.740	L1-2
597	1	4	16	466	213	34	0.2199E-04	0.1767E-04	0.803	0.1431E-04	0.651	L1-2
599	1	4	36	486	218	45	0.2335E-04	0.2144E-04	0.918	0.1918E-04	0.821	L1-2
601	1	4	56	506	204	41	0.2787E-04	0.2181E-04	0.782	0.1887E-04	0.677	L1-2
603	1	4	76	526	249	30	0.2734E-04	0.2301E-04	0.841	0.1897E-04	0.694	L1-2
605	1	4	96	546	212	41	0.2244E-04	0.1948E-04	0.868	0.1540E-04	0.686	L1-2
607	1	4	116	566	221	41	0.3107E-04	0.2849E-04	0.917	0.2339E-04	0.753	L1-2
609	1	4	136	586	214	47	0.2882E-04	0.2566E-04	0.890	0.2029E-04	0.704	L1-2
610	1	4	146	596	213	42	0.3409E-04	0.2821E-04	0.828	0.2206E-04	0.647	L1-2
617	1	5	6	606	217	12	0.2261E-04	0.1863E-04	0.824	0.1502E-04	0.664	L1-3
619	1	5	26	626	190	38	0.1320E-04	0.1115E-04	0.845	0.9069E-05	0.687	L1-2
620	1	5	36	636	209	- 3	0.2120E-04	0.1424E-04	0.672	0.1094E-04	0.516	L1-2
621	1	5	46	646	207	28	0.2362E-04	0.1662E-04	0.703	0.1419E-04	0.601	L1-2
622	1	5	56	656	201	25	0.3032E-04	0.2318E-04	0.765	0.2028E-04	0.669	L1-2
623	1	5	66	666	204	-12	0.2282E-04	0.2111E-04	0.925	0.1811E-04	0.794	L1-2
624	1	5	76	676	207	-24	0.1960E-04	0.1571E-04	0.801	0.1300E-04	0.663	L1-2
625	1	5	86	686	230	- 2	0.7069E-05	0.8025E-05	1.135	0.5878E-05	0.832	L5
626	1	5	96	696	276	-45	0.4260E-05	0.5473E-05	1.285	0.5042E-05	1.184	L1-3
627	1	5	106	706	257	-51	0.7136E-05	0.8119E-05	1.138	0.8212E-05	1.151	L1-2
629	1	5	126	726	249	-28	0.6293E-05	0.7374E-05	1.172	0.6298E-05	1.001	L1-2
631	1	5	146	746	263	-38	0.5295E-05	0.5652E-05	1.067	0.4454E-05	0.841	L1-2
611	1	6	6	756	271	-50	0.1245E-04	0.1510E-04	1.213	0.1173E-04	0.942	L1-3
613	1	6	26	776	271	-50	0.1867E-04	0.1914E-04	1.025	0.1469E-04	0.787	L1-2
615	1	6	46	796	287	-51	0.1865E-04	0.2002E-04	1.073	0.1543E-04	0.827	L1-2
616	1	6	54	804	282	-48	0.1572E-04	0.1477E-04	0.939	0.1338E-04	0.851	L1-2
632	2	1	11	1171	27	-31	0.1078E-04	0.1050E-04	0.974	0.1013E-04	0.939	L1-2,F
633	2	1	19	1179	29	-44	0.1477E-04	0.1693E-04	1.146	0.1391E-04	0.942	L1-2
635	2	1	36	1196	34	-57	0.2128E-04	0.2088E-04	0.981	0.1750E-04	0.822	L1-2
637	2	1	56	1216	21	-42	0.2047E-04	0.2182E-04	1.066	0.1770E-04	0.865	L1-2
639	2	1	76	1236	24	-56	0.1025E-04	0.9172E-05	0.895	0.1001E-04	0.977	L1-2
641	2	1	96	1256	29	-50	0.2546E-04	0.2589E-04	1.017	0.1962E-04	0.770	L1-2
643	2	1	116	1276	31	-40	0.1574E-04	0.1830E-04	1.163	0.1358E-04	0.863	L1-2
645	2	1	136	1296	26	-34	0.1232E-04	0.1390E-04	1.128	0.1150E-04	0.933	L1-2
647	2	2	6	1316	19	-31	0.1191E-04	0.1376E-04	1.156	0.1191E-04	1.001	L1-2
649	2	2	26	1336	37	-48	0.9595E-05	0.1018E-04	1.061	0.9212E-05	0.960	L1-2
651	2	2	46	1356	32	-39	0.1742E-04	0.1991E-04	1.143	0.1521E-04	0.873	L1-2
653	2	2	66	1376	19	-53	0.1250E-04	0.1145E-04	0.916	0.1021E-04	0.817	L1-2
655	2	2	86	1396	27	-48	0.2542E-04	0.2544E-04	1.001	0.2083E-04	0.819	L1-2

Table 2. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
657	2	2	106	1416	25	-49	0.1801E-04	0.2198E-04	1.220	0.1756E-04	0.975	L1-2
659	2	2	126	1436	29	-49	0.2017E-04	0.2135E-04	1.059	0.1770E-04	0.877	L1-2
661	2	2	146	1456	26	-51	0.1156E-04	0.1279E-04	1.106	0.1156E-04	0.999	L1-2
663	2	3	15	1475	357	-46	0.5785E-05	0.8371E-05	1.447	0.6624E-05	1.145	L1-2
664	2	3	26	1486	10	-47	0.1105E-04	0.1287E-04	1.165	0.9473E-05	0.857	L1-2
665	2	3	36	1496	168	13	0.8638E-05	0.4473E-05	0.518	0.3425E-05	0.396	L1-2
667	2	3	56	1516	189	49	0.2157E-04	0.1943E-04	0.900	0.1406E-04	0.652	L1-2
669	2	3	76	1536	181	13	0.2631E-04	0.2115E-04	0.804	0.1806E-04	0.687	L1-2
673	2	4	46	1656	196	-48	0.2022E-04	0.2223E-04	1.099	0.1728E-04	0.855	L1-2
674	2	4	56	1666	193	-46	0.1308E-04	0.1492E-04	1.141	0.1037E-04	0.793	L1-2
675	2	4	66	1676	189	-49	0.1750E-04	0.2045E-04	1.168	0.1697E-04	0.970	L1-2
676	2	4	76	1686	182	-54	0.1505E-04	0.1475E-04	0.981	0.1231E-04	0.818	L1-2
677	2	4	86	1696	184	-41	0.1552E-04	0.1962E-04	1.265	0.1449E-04	0.934	L1-2
678	2	4	96	1706	163	-49	0.2233E-04	0.2051E-04	0.918	0.1735E-04	0.777	L1-2
679	2	4	106	1716	188	-53	0.1512E-04	0.1487E-04	0.984	0.1183E-04	0.782	L1-2
680	2	4	116	1726	188	-44	0.2453E-04	0.2465E-04	1.005	0.1914E-04	0.780	L1-2
681	2	4	126	1736	184	-51	0.1784E-04	0.1833E-04	1.028	0.1521E-04	0.853	L1-2
682	2	4	136	1746	194	-68	0.2104E-04	0.1764E-04	0.838	0.1417E-04	0.674	L1-2
683	2	4	146	1756	171	-48	0.1604E-04	0.1551E-04	0.967	0.1305E-04	0.814	L1-2
684	2	5	6	1766	164	-68	0.8324E-05	0.9673E-05	1.162	0.7930E-05	0.953	L1-2
685	2	5	16	1776	158	-87	0.3707E-05	0.6104E-05	1.647	0.4410E-05	1.190	L1-3
686	2	5	25	1786	200	-36	0.7980E-05	0.9018E-05	1.130	0.6499E-05	0.814	L1-2
687	2	5	36	1796	188	-53	0.1391E-04	0.1539E-04	1.107	0.1239E-04	0.891	L1-2
688	2	5	46	1806	299	-72	0.1354E-04	0.1666E-04	1.230	0.1155E-04	0.853	L1-3
689	2	5	56	1816	298	-71	0.1067E-04	0.1317E-04	1.235	0.1127E-04	1.056	L1-2
690	2	5	66	1826	139	-80	0.1002E-04	0.1309E-04	1.306	0.8905E-05	0.889	L1-2
691	2	5	76	1836	131	-63	0.1352E-05	0.1759E-05	1.300	0.1262E-05	0.933	L1-2
692	2	5	86	1846	30	46	0.1361E-04	0.9511E-05	0.699	0.7171E-05	0.527	L1
693	2	5	96	1856	5	40	0.2262E-04	0.1549E-04	0.685	0.1261E-04	0.557	L1-2
694	2	5	106	1866	3	49	0.1896E-04	0.1098E-04	0.579	0.9542E-05	0.503	L1-2
695	2	5	116	1876	4	47	0.1756E-04	0.1239E-04	0.706	0.1070E-04	0.609	L1-2
696	2	5	126	1886	13	36	0.2871E-04	0.2372E-04	0.826	0.1633E-04	0.569	L1-2
697	2	5	136	1896	357	50	0.2859E-04	0.2381E-04	0.833	0.1962E-04	0.686	L1-2
698	2	5	146	1906	5	50	0.1472E-04	0.1212E-04	0.823	0.6915E-05	0.470	L1-2
699	2	6	6	1916	3	51	0.2533E-04	0.1826E-04	0.721			L1-2
700	2	6	16	1926	6	55	0.2626E-04	0.2161E-04	0.823	0.1568E-04	0.597	L1-2
701	2	6	26	1936	3	41	0.2142E-04	0.1668E-04	0.779	0.1250E-04	0.584	L1-2
702	2	6	36	1946	8	41	0.2510E-04	0.1921E-04	0.765	0.1393E-04	0.555	L1-2
703	2	6	46	1956	5	42	0.2327E-04	0.1834E-04	0.788	0.1253E-04	0.538	L1-2
704	2	6	56	1966	4	47	0.2256E-04	0.1510E-04	0.669	0.1198E-04	0.531	L1-2
705	2	6	66	1976	360	51	0.3137E-04	0.2370E-04	0.756	0.1902E-04	0.606	L1-2
706	2	6	76	1986	4	46	0.1875E-04	0.1141E-04	0.608	0.8260E-05	0.441	L1-2
707	2	6	86	1996	168	-47	0.3568E-05	0.4439E-05	1.244	0.4510E-05	1.264	L1-2
708	2	6	96	2006	179	-47	0.7811E-05	0.1175E-04	1.505	0.9735E-05	1.246	L1-2
709	2	6	106	2016	7	49	0.1830E-04	0.1102E-04	0.602	0.6503E-05	0.355	L1-2
710	2	6	116	2026	0	52	0.2458E-04	0.1520E-04	0.619	0.9541E-05	0.388	L1-2
711	2	6	126	2036	119	-19	0.7439E-05	0.8339E-06	0.112	0.5363E-06	0.072	L3
712	2	6	136	2046	170	-53	0.6789E-05	0.1039E-04	1.531	0.9320E-05	1.373	L1-2
713	2	6	146	2056	56	-62	0.5867E-05	0.6582E-06	0.112	0.4942E-06	0.084	L2-3
714	2	7	6	2066	341	66	0.1066E-04	0.7012E-05	0.658	0.4429E-05	0.416	L1-5
715	2	7	16	2076	346	48	0.7562E-05	0.5553E-05	0.734	0.4033E-05	0.533	L1-2
716	2	7	26	2086	288	77	0.1425E-04	0.9334E-05	0.655	0.6670E-05	0.468	L1-7
717	2	7	36	2096	347	66	0.2024E-04	0.1377E-04	0.681	0.9337E-05	0.461	L1-2
718	3	1	6	2116	298	33	0.9963E-05	0.4398E-05	0.441	0.2794E-05	0.280	L1-2
719	3	1	16	2126	309	42	0.1476E-04	0.6263E-05	0.424	0.4549E-05	0.308	L1-2
720	3	1	26	2136	120	-65	0.3283E-05	0.4179E-05	1.273	0.2981E-05	0.908	L1-2
721	3	1	36	2146	128	-54	0.8681E-06	0.5440E-05	6.266	0.3948E-05	4.548	L1-2
722	3	1	86	2196	329	45	0.9741E-05	0.6017E-05	0.618	0.3296E-05	0.338	L1-2
723	3	1	46	2156	146	-50	0.2864E-05	0.6617E-05	2.310	0.5712E-05	1.994	L1-2
724	3	1	56	2166	142	-56	0.2264E-05	0.6562E-05	2.898	0.5742E-05	2.536	L1-2

Table 2. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
725	3	1	66	2176	140	-53	0.2922E-05	0.6975E-05	2.387	0.5628E-05	1.926	L1-2
726	3	1	76	1996	169	-73	0.5738E-05	0.3001E-06	0.052	0.3689E-06	0.064	L1-2
727	3	1	96	2016	342	42	0.9242E-05	0.4551E-05	0.492	0.2827E-05	0.306	L1-2
728	3	1	106	2026	134	-53	0.3855E-05	0.2564E-05	0.665	0.2377E-05	0.617	L1-2
729	3	1	116	2036	152	-54	0.1359E-05	0.5320E-05	3.915	0.3883E-05	2.858	L1-2
730	3	1	126	2046	149	-42	0.2032E-05	0.7549E-05	3.715	0.5870E-05	2.889	L1-2
731	3	1	136	2056	154	-54	0.2386E-05	0.6185E-05	2.592	0.4220E-05	1.769	L1-2
732	3	1	146	2066	332	37	0.1283E-04	0.5884E-05	0.459	0.4390E-05	0.342	L1-2
733	3	2	6	2076	351	41	0.1747E-04	0.9174E-05	0.525	0.5492E-05	0.314	L1-2
734	3	2	16	2086	337	45		0.6428E-05		0.4346E-05		L1-2
735	3	2	26	2096	347	53	0.1141E-04	0.6032E-05	0.529	0.3613E-05	0.317	L1-2
736	3	2	36	2106	345	39	0.1153E-04	0.6126E-05	0.531	0.4434E-05	0.385	L1-2
737	3	2	46	2116	352	47	0.1324E-04	0.7074E-05	0.534	0.5032E-05	0.380	L1-2
738	3	2	56	2126	351	52	0.1262E-04	0.7451E-05	0.590	0.3827E-05	0.303	L1-2
739	3	2	66	2136	161	-49	0.4161E-05	0.1638E-05	0.394	0.1438E-05	0.346	L1-2
740	3	2	76	2206	153	-49	0.4359E-05	0.2628E-05	0.603	0.2410E-05	0.553	L1-2
741	3	2	86	2216	146	-52	0.2801E-05	0.5005E-05	1.787	0.3587E-05	1.281	L1-2
742	3	2	96	2226	153	-49	0.1209E-05	0.3176E-05	2.627	0.2650E-05	2.192	L1-2
743	3	2	106	2236	162	-43	0.1169E-05	0.3787E-05	3.241	0.3408E-05	2.916	L1-2
744	3	2	116	2246	169	-56	0.1089E-05	0.5882E-05	5.403	0.4196E-05	3.854	L1-2
745	3	2	126	2256	161	-36	0.1544E-05	0.4406E-05	2.854	0.3693E-05	2.392	L1-2
746	3	2	136	2266	161	-37	0.2920E-05	0.6511E-05	2.230	0.4978E-05	1.705	L1-2
747	3	2	146	2276	162	-38	0.2444E-05	0.6976E-05	2.855	0.5204E-05	2.129	L1-2
748	3	3	6	2286	186	41	0.5170E-05	0.9350E-05	1.808	0.5610E-05	1.085	L1-2
749	3	3	16	2296	182	-47	0.2157E-05	0.2741E-05	1.271	0.2042E-05	0.947	L1-2
750	3	3	26	2306	161	-37	0.2856E-05	0.1763E-05	0.617	0.1365E-05	0.478	L1-2
751	3	3	36	2316	158	-33	0.4506E-05	0.7157E-05	1.588	0.5529E-05	1.227	L1-2
752	3	3	46	2326	106	16	0.9670E-05	0.6476E-05	0.670	0.4699E-05	0.486	L1-4
765	3	6	26	2452	355	54	0.1255E-04	0.1671E-05	0.133	0.6691E-06	0.053	L1
766	3	6	46	2462	131	-44	0.3928E-05	0.5506E-05	1.402	0.4631E-05	1.179	L1-2
767	3	6	66	2492	63	74	0.1237E-04	0.9983E-06	0.081	0.3768E-06	0.030	L1
768	3	6	86	2512	316	55	0.1670E-04	0.5049E-05	0.302	0.3067E-05	0.184	L1-2
769	3	6	106	2532	134	-46	0.7143E-05	0.5366E-05	0.751	0.4295E-05	0.601	L1-2
770	3	6	126	2552	139	4	0.1578E-04	0.1296E-05	0.082	0.9644E-06	0.061	L3-4
771	3	6	146	2572	117	-25	0.7950E-05	0.2499E-05	0.314	0.2611E-05	0.328	L1-2
772	3	7	6	2582	120	66	0.1303E-04	0.1070E-05	0.082	0.3924E-06	0.030	L1-2
773	3	7	26	2602	345	63	0.1582E-04	0.1490E-05	0.094	0.5079E-06	0.032	L1
774	3	7	46	2622	324	52	0.1407E-04	0.3479E-05	0.247	0.1844E-05	0.131	L1-2
775	4	3	106	3416	12	18	0.1480E-04	0.6264E-05	0.423	0.3760E-05	0.254	L1-3
776	4	3	126	3436	7	-11	0.8827E-05	0.5145E-05	0.583	0.3506E-05	0.397	L1-3
777	4	3	146	3456	7	19	0.1344E-04	0.3097E-05	0.230	0.1580E-05	0.118	L1-3
778	4	4	6	3466	2	16	0.1704E-04	0.4060E-05	0.238	0.2065E-05	0.121	L1-3
779	4	4	26	3486	3	12	0.1450E-04	0.3586E-05	0.247	0.1824E-05	0.126	L1-3
780	4	4	46	3506	353	23	0.1517E-04	0.3571E-05	0.235	0.1805E-05	0.119	L1-3
781	4	4	66	3526	5	22	0.1199E-04	0.2473E-05	0.206	0.1354E-05	0.113	L1-3
782	4	4	86	3546	337	32	0.1223E-04	0.3474E-05	0.284	0.1906E-05	0.156	L1-3
783	4	4	106	3566	342	29	0.1447E-04	0.3357E-05	0.232	0.1996E-05	0.138	L1-3
784	4	4	126	3586	342	37	0.1759E-04	0.4362E-05	0.248	0.2146E-05	0.122	L1-2
785	4	4	146	3606	11	17	0.1496E-04	0.3091E-05	0.207	0.1777E-05	0.119	L1-3
786	4	5	6	3616	327	-15	0.1456E-04	0.5362E-05	0.368	0.3025E-05	0.208	L1-2
787	4	5	26	3636	355	17	0.1528E-04	0.3090E-05	0.202	0.1789E-05	0.117	L1-3
788	4	5	46	3656	349	24	0.2030E-04	0.2924E-05	0.144	0.1784E-05	0.088	L1-3
789	4	5	66	3676	18	-18	0.1606E-04	0.2439E-05	0.152	0.1842E-05	0.115	L1-3
790	4	5	86	3696	27	-25	0.1653E-04	0.4022E-05	0.243	0.3460E-05	0.209	L1-3
791	4	5	106	3716	5	-18	0.1594E-04	0.6014E-05	0.377	0.4083E-05	0.256	L1-3
792	4	5	126	3736				1.5229E-05		2.3684E-05		U
793	4	5	146	3756	354	16	0.1007E-04	0.5496E-05	0.546	0.3969E-05	0.394	L1-3
794	4	6	6	3766	360	-11	0.1045E-04	0.5869E-05	0.562	0.3308E-05	0.317	L1-3
795	4	6	26	3786	6	-14	0.8672E-05	0.5609E-05	0.647	0.3583E-05	0.413	L1-3
796	4	6	46	3806	352	-10	0.8328E-05	0.7404E-05	0.889	0.4629E-05	0.556	L1-4

Table 2. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
797	4	6	66	3826	2	-49	0.8676E-05	0.8458E-05	0.975	0.5881E-05	0.678	L1-2
798	4	6	86	3846	10	-33	0.1688E-05	0.5970E-05	3.536	0.4756E-05	2.817	L1-2
799	4	6	106	3866	31	-15	0.6964E-05	0.6753E-05	0.970	0.4012E-05	0.576	L1-2
800	4	6	126	3886	26	- 5	0.1244E-04	0.1066E-04	0.857	0.6970E-05	0.560	L1-2
801	4	6	146	3906	270	12	0.3239E-04	0.1363E-04	0.421	0.9374E-05	0.289	L1-7
802	4	7	6	3916	269	56	0.3634E-04	0.1803E-04	0.496	0.1285E-04	0.353	L1-2
803	4	7	26	3936	336	37	0.2354E-04	0.5384E-05	0.229	0.3126E-05	0.133	L1-2
804	4	7	46	3957	54	42	0.1938E-04	0.6843E-05	0.353	0.5074E-05	0.262	L1-2
806	5	2	6	4016	103	29	0.1632E-04	0.8228E-05	0.504	0.6278E-05	0.385	L1-3
807	5	2	26	4036	105	46	0.3435E-04	0.1370E-04	0.399	0.9721E-05	0.283	L1-2
808	5	2	46	4056	97	49	0.3040E-04	0.1011E-04	0.333	0.5747E-05	0.189	L1-2
809	5	2	67	4077	90	16	0.2331E-04	0.8137E-05	0.349	0.4794E-05	0.206	L1-2
810	5	2	87	4097	110	18	0.2265E-04	0.7602E-05	0.336	0.5233E-05	0.231	L1-3
811	5	2	107	4117	105	32	0.1540E-04	0.6051E-05	0.393	0.3511E-05	0.228	L1-2
812	5	2	126	4136	121	28	0.1724E-04	0.3696E-05	0.214	0.2494E-05	0.145	L1-2
813	5	2	146	4156	98	60	0.2646E-04	0.6526E-05	0.247	0.4259E-05	0.161	L1-2
814	5	3	6	4166	103	58	0.2998E-04	0.9982E-05	0.333	0.6253E-05	0.209	L1-2
815	5	3	26	4186	3	64	0.1633E-04	0.5688E-05	0.348	0.3578E-05	0.219	L1-2
816	5	3	46	4206	79	-23	0.1483E-04	0.5437E-05	0.367	0.2913E-05	0.196	L1
817	5	3	66	4226	261	2	0.1789E-04	0.9223E-05	0.516	0.2755E-05	0.154	L1-3
818	5	3	86	4246	89	-13	0.1618E-04	0.5585E-05	0.345	0.3848E-05	0.238	L1-3
819	5	3	106	4266	97	20	0.4027E-04	0.1294E-04	0.321	0.5921E-05	0.147	L1-2
820	5	3	126	4286	289	44	0.1613E-04	0.5407E-05	0.335	0.5262E-05	0.326	L1-2
821	5	3	146	4306	74	24	0.1564E-04	0.1270E-04	0.812	0.9839E-05	0.629	L1-2
822	5	4	6	4316	293	-21	0.1226E-04	0.1508E-04	1.230	0.1150E-04	0.939	L1-2
823	5	4	26	4336	107	32	0.4144E-04	0.1154E-04	0.278	0.5199E-05	0.125	L1-2
824	5	4	46	4356	85	36	0.2586E-04	0.9017E-05	0.349	0.4917E-05	0.190	L1-2
825	5	4	66	4376			0.1242E-04	1.1595E-05	0.128	2.8791E-06	0.071	U
826	5	4	86	4396	273	-13	0.2668E-04	0.2576E-04	0.965	0.1256E-04	0.471	L1-2
827	5	4	106	4416	96	13	0.2650E-04	0.4960E-05	0.187	0.7229E-06	0.027	L1
828	5	4	126	4436	96	41	0.3056E-04	0.8733E-05	0.286	0.2449E-05	0.080	L1-2
829	5	4	146	4456	315	44	0.2864E-04	0.5956E-05	0.208	0.4706E-05	0.164	L1-2
830	5	5	6	4466	61	43	0.2244E-04	0.2971E-05	0.132	0.8105E-06	0.036	L1
831	5	5	26	4486	94	53	0.2914E-04	0.1132E-04	0.389	0.4192E-05	0.144	L1-2
832	5	5	46	4506	301	2	0.7380E-05	0.3889E-05	0.527	0.3905E-05	0.529	L1-2
833	5	5	66	4526	8	-46	0.1286E-04	0.1913E-05	0.149	0.2087E-05	0.162	L1-2
834	5	5	86	4546	273	- 6	0.1232E-04	0.1129E-04	0.917	0.6796E-05	0.552	L1-2
835	5	5	107	4567	109	13	0.4942E-04	0.2692E-04	0.545	0.1636E-04	0.331	L1-3
836	5	5	126	4586	257	- 9	0.1268E-04	0.3407E-05	0.269	0.2177E-05	0.172	L1-4
837	5	5	146	4606	281	-34	0.9651E-05	0.1212E-04	1.256	0.5552E-05	0.575	L1-2
838	5	6	6	4616	262	-17	0.1514E-04	0.1603E-04	1.059	0.1013E-04	0.669	L1-3
839	5	6	26	4636	259	1	0.1811E-04	0.1821E-04	1.006	0.1091E-04	0.603	L1-3
840	5	6	46	4656	283	0	0.1976E-04	0.2064E-04	1.045	0.1061E-04	0.537	L1-2
841	5	6	66	4676	280	- 6	0.2812E-04	0.2301E-04	0.818	0.1517E-04	0.540	L1-2
842	5	6	86	4696	243	- 3	0.1420E-04	0.9403E-05	0.662	0.4469E-05	0.315	L1-2
843	5	6	106	4716	57	19	0.2690E-04	0.6006E-05	0.223	0.4380E-05	0.163	L1-2
844	6	1	126	5122	26	-57	0.2155E-04	0.8238E-05	0.382	0.6188E-05	0.287	L1-2
845	6	1	146	5142	263	-22	0.3091E-04	0.6020E-05	0.195	0.3932E-05	0.127	L1-2
846	6	2	6	5162	312	- 8	0.2003E-04	0.5521E-05	0.276	0.3436E-05	0.171	L1-2
847	6	2	26	5182	47	-12	0.3040E-04	0.7982E-05	0.263	0.4810E-05	0.158	L1-2
848	6	2	46	5202	232	30	0.5203E-04	0.1352E-04	0.260	0.8374E-05	0.161	L1-2
849	6	2	66	5222	237	17	0.5246E-04	0.1408E-04	0.268	0.1014E-04	0.193	L1-2
850	6	2	86	5242	278	-13	0.3722E-04	0.4717E-05	0.127	0.2590E-05	0.070	L1-2
851	6	2	106	5262	244	46	0.3808E-04	0.5654E-05	0.148	0.3243E-05	0.085	L1-2
852	6	2	126	5282	261	20	0.3825E-04	0.3968E-05	0.104	0.2852E-05	0.075	L1-4
853	6	2	146	5302	52	7	0.3257E-04	0.3611E-05	0.111	0.2009E-05	0.062	L1-2
854	6	3	6	5312	27	-19	0.2570E-04	0.7921E-05	0.308	0.5690E-05	0.221	L1-2
855	6	3	26	5322	257	40	0.3434E-04	0.4186E-05	0.122	0.3185E-05	0.093	L1-2
856	6	3	46	5342	131	58	0.3327E-04	0.3897E-05	0.117	0.2475E-05	0.074	L1-2
857	6	3	67	5363	260	20	0.4743E-04	0.1023E-04	0.216	0.6504E-05	0.137	L1-2

Table 2. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	J_{200} (emu)	J_{200}/J_0	Note
858	6	3	86	5382	32	2	0.3146E-04	0.6622E-05	0.211	0.3959E-05	0.126	L1-2
859	6	3	106	5402	48	-13	0.2716E-04	0.7798E-05	0.287	0.5935E-05	0.219	L1-2
860	6	3	126	5422	70	-25	0.2424E-04	0.1590E-04	0.656	0.1150E-04	0.474	L1-2
861	6	3	146	5442	262	-55	0.3211E-04	0.5615E-05	0.175	0.2364E-05	0.074	L1-2
862	6	4	6	5452	324	13	0.2343E-04	0.4006E-05	0.171	0.2551E-05	0.109	L1
863	6	4	26	5472	215	38	0.3452E-04	0.3926E-05	0.114	0.1129E-05	0.033	L1
864	6	4	46	5492	258	12	0.5312E-04	0.1479E-04	0.278	0.1070E-04	0.201	L1-2
865	6	4	66	5512	87	-22	0.3780E-04	0.8017E-06	0.021	0.2888E-05	0.076	L1-3
866	6	4	86	5532	253	- 5	0.4840E-04	0.4384E-05	0.091	0.1542E-05	0.032	L1
867	6	4	106	5552	304	27	0.4988E-04	0.1199E-04	0.240	0.8632E-05	0.173	L1-2
868	6	4	146	5592	275	17	0.7992E-04	0.4446E-04	0.556	0.3180E-04	0.398	L1-2
869	6	5	55	5651	273	22	0.5306E-04	0.1666E-04	0.314	0.1231E-04	0.232	L1-2
870	6	5	86	5682	275	19	0.7436E-04	0.3535E-04	0.475	0.2620E-04	0.352	L1-2
871	6	5	106	5702	306	27	0.3562E-04	0.5017E-05	0.141	0.2708E-05	0.076	L1-2
872	6	5	126	5722	83	-11	0.2257E-04	0.1265E-04	0.561	0.9275E-05	0.411	L1-2
873	6	5	144	5740	290	7	0.3917E-04	0.1761E-04	0.450	0.1277E-04	0.326	L1-2
874	6	6	47	5793	278	4	0.4097E-04	0.1252E-04	0.306	0.6730E-05	0.164	L1-3
875	6	6	76	5822	57	- 6	0.3526E-04	0.1775E-05	0.050	0.3466E-05	0.098	L1-2
876	6	6	136	5882	69	-24	0.2648E-04	0.3838E-05	0.145	0.4448E-05	0.168	L1-2
877	7	3	145	6245	162	-21	0.3007E-04	0.4494E-04	1.494	0.3157E-04	1.050	L1-2
878	7	4	91	6341	152	- 4	0.2487E-04	0.6307E-05	0.254	0.6090E-05	0.245	L1-2
879	7	4	128	6378	339	12	0.3786E-04	0.5319E-05	0.140	0.2401E-05	0.063	L1
880	7	5	79	6479	119	-14	0.2868E-04	0.2459E-04	0.858	0.1776E-04	0.619	L1-2
881	7	6	26	6576	103	-17	0.1395E-04	0.2372E-04	1.701	0.1821E-04	1.305	L1-2
882	7	6	46	6596	115	70	0.1495E-04	0.1041E-04	0.697	0.9306E-05	0.623	L1-2
883	7	6	89	6639	275	5	0.3872E-04	0.1461E-04	0.377	0.8647E-05	0.223	L1-2
884	7	7	30	6730	260	- 5	0.1769E-04	0.1442E-04	0.815	0.1187E-04	0.671	L1-2
885	8	2	81	6976	293	3	0.4411E-04	0.2268E-04	0.514	0.1260E-04	0.286	L1-2
886	8	3	29	7074	318	- 2	0.3063E-04	0.8459E-05	0.276	0.4129E-05	0.135	L1-2
887	8	3	65	7110	316	5	0.3969E-04	0.1472E-04	0.371	0.7835E-05	0.197	L1-2
888	8	3	96	7141	310	13	0.5152E-04	0.2096E-04	0.407	0.1303E-04	0.253	L1-2
889	8	4	21	7216	333	8	0.6136E-04	0.3187E-04	0.519	0.1644E-04	0.268	L1-2
890	8	4	41	7236	326	13	0.4531E-04	0.1506E-04	0.332	0.7976E-05	0.176	L1-2
891	8	4	99	7294	132	- 6	0.1723E-04	0.3324E-05	0.193	0.2161E-05	0.125	L1-2
892	8	5	58	7403	142	-20	0.3787E-04	0.3818E-04	1.008	0.2331E-04	0.615	L1-2
893	8	5	142	7487	136	-15	0.1176E-04	0.7574E-05	0.644	0.5679E-05	0.483	L1-2
894	8	6	44	7539	330	13	0.1350E-04	0.2052E-04	1.520	0.1207E-04	0.894	L1-2

Note: L = demagnetization level or levels (x 100; vector averages) used to define declination and inclination.
U = magnetically unstable samples. F = flow-in, based on shipboard visual descriptions.

still high enough to prevent the "swamping" of detrital remanence by chemical remanence, as appears to have occurred at Site 576.

The NRM (J_0) and J_{100} values correlate very well for the magnetically stable samples above about 145 m (Fig. 10). At greater depths, however, NRM values increase, whereas J_{100} values approach zero. The J_{100}/J_0 ratio (Fig. 10) shows a tight clustering of values above about 100 m, where sedimentation rates exceed 12 m/m.y., increased scatter but a good continuation of the shallower trend to about 145 m, then scattered, very low values to the base of the section.

DISCUSSION

The magnetic data at both Sites 576 and 578 yield detailed age-depth curves (Figs. 2, 8). Differentiation of these curves yields sedimentation rates as a function of time (Fig. 11).

In both cases, the past 2 m.y. has been a period of increased sedimentation, a phenomenon that has been observed across the North Pacific and that has been attributed to eolian transport of fine-grained glacial debris from Asia and, to a lesser extent, from North America. This explanation is supported by the remarkable similarity of the rate increases at Sites 576 and 578 (about 5-6 $m/m.y.^2$ during the Quaternary, in each case). Such a uniform increase is unlikely to reflect either changes in bottom transport, given the separation of the two sites by Shatsky Rise, or changes in surface transport, given the upstream distance to source areas, particularly at Site 576. The uniformity of the increase also is in striking contrast to the very different accumulation rate his-

Table 3. Magnetization of Site 576 samples after AF demagnetization at intensities above 200 Oe.

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	Demagnetization Level (OE)	J (emu)	J/J_0
36	2	1	96	791	47	-51	300	0.1745E-04	0.689
							400	0.1310E-04	0.517
45	2	2	36	881	263	19	300	0.1244E-05	0.199
49	2	2	76	921	278	54	300	0.1560E-04	0.582
							400	0.1185E-04	0.442
53	2	2	116	961	267	-38	250	0.6133E-06	0.214
							300	0.3696E-06	0.129
							400	0.6096E-06	0.212
97	2	5	106	1401	287	-69	300	0.5571E-05	0.756
99	2	5	126	1421	154	-67	300	0.1380E-04	0.644
101	2	5	146	1441	185	-84	300	0.1349E-04	0.606
							400	0.1066E-04	0.479
103	2	6	16	1461	75	-79	300	0.1429E-04	0.656
109	2	6	76	1521	22	14	300	0.1893E-05	0.499
110	2	6	86	1531	20	-20	300	0.7121E-05	0.501
111	2	6	96	1541	6	28	300	0.6299E-05	0.435
113	2	6	116	1561	329	19	300	0.5379E-05	0.575
114	2	6	126	1571	335	19	300	0.2906E-05	0.497
							400	0.1669E-05	0.286
179	3	4	146	1581	162	40	300	0.3612E-06	0.065
189	4	1	76	1856			300	0.2121E-05	0.309
							400	0.1489E-04	2.171
							500	0.1091E-05	0.159
							600	0.1138E-05	0.166
							700	0.8307E-06	0.121
							800	0.6931E-06	0.101
192	4	1	106	1886	146	51	300	0.1328E-04	0.346
							400	0.8800E-05	0.229
196	4	1	146	1926	211	-54	300	0.1115E-04	0.319
215	4	3	36	2116	165	54	300	0.68200-05	
							400	0.40900-05	
219	4	3	76	2156	7	51	300	0.4559E-05	1.791
							400	0.2523E-05	0.991
							500	0.1432E-05	0.562
							600	0.1092E-05	0.429
221	4	3	96	2176	354	-55	300	0.7906E-05	1.212
							400	0.4623E-05	0.709
							500	0.3139E-05	0.481
241	4	4	146	2376	308	- 4	300	0.5650E-05	2.212
							400	0.3054E-05	1.196
							500	0.2011E-05	0.787
							600	0.1389E-05	0.544
							700	0.1316E-05	0.515
252	4	5	106	2486	304	- 3	300	0.2457E-05	0.419
254	4	5	126	2506	3	-52	300	0.5584E-05	1.113
256	4	5	146	2526	360	-52	300	0.4065E-05	0.628
258	4	6	16	2546	349	-53	300	0.5221E-05	0.668
262	4	6	56	2586	353	-45	300	0.4812E-05	0.450
263	4	6	66	2596	333	-30	300	0.2324E-05	0.120
264	4	6	76	2606	340	-20	300	0.3839E-05	0.191
							400	0.1731E-05	0.086
265	4	6	86	2616	9	-66	300	0.5058E-05	0.497
							400	0.3182E-05	0.313
266	4	6	96	2626	335	-45	300	0.2418E-05	0.090
267	4	6	106	2636	286	-38	300	0.1486E-05	0.053
268	4	6	116	2646	21	-13	300	0.2102E-05	0.085
							400	0.7508E-06	0.031
269	4	6	126	2656	294	-24	300	0.2051E-06	0.234

Table 3. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	Demagnetization Level (OE)	J (emu)	J/J_0
270	4	6	136	2666	281	-10	300	0.9917E-06	0.030
271	4	6	146	2676	309	-48	300	0.1365E-06	0.055
272	4	7	6	2686	282	- 7	300	0.2052E-05	0.068
273	4	7	16	2696	265	-20	300	0.2310E-06	0.116
274	4	7	26	2706	357	-40	300	0.1101E-05	0.043
275	4	7	36	2716	284	-14	300	0.1790E-05	0.097
							250	0.1656E-06	0.088
							300	0.8989E-06	0.480
276	4	7	46	2726	77	17	300	0.1772E-05	0.064
							400	0.1774E-05	0.064
							400	0.2038E-05	0.073
							500	0.1865E-05	0.067
							500	0.1994E-05	0.072
278	5	1	46	2866	148	-78	300	0.3144E-05	0.341
							400	0.1339E-05	0.145
280	5	1	66	2886	220	-69	300	0.4670E-05	0.445
281	5	1	76	2896	225	-71	300	0.5182E-05	0.898
282	5	1	86	2906	233	-78	300	0.4674E-05	0.545
284	5	1	106	2926	64	13	300	0.1790E-05	0.097
285	5	1	116	2936	71	6	300	0.1225E-05	0.090
							300	0.1729E-05	0.128
							400	0.1133E-05	0.084
286	5	1	126	2946	95	-37	300	0.7718E-06	0.055
287	5	1	136	2956	87	- 4	300	0.7589E-06	0.072
							400	0.6077E-06	0.058
288	5	1	146	2966	48	3	300	0.9601E-06	0.066
302	5	5	130	3240	308	- 5	300	0.2997E-05	0.107
							400	0.1415E-05	0.051
305	5	6	16	3276	287	4	300	0.8436E-06	0.028
306	5	6	26	3286	255	14	300	0.1515E-05	0.064
308	5	6	46	3306	305	30	300	0.1280E-05	0.058
							400	0.9700E-06	0.044
309	5	6	56	3316	315	-14	300	0.1652E-05	0.070
							400	0.5543E-06	0.024
							500	0.1300E-05	0.055
311	5	6	76	3336	294	-22	300	0.1126E-05	0.056
312	5	6	86	3346	293	- 9	300	0.6740E-06	0.046
313	5	6	96	3356	301	26	300	0.8159E-06	0.029
314	5	6	107	3367	265	- 9	300	0.6934E-06	0.061
							400	0.3996E-06	0.035
							400	0.7917E-06	0.070
315	5	6	116	3376	303	21	300	0.1054E-05	0.044
316	5	6	126	3386	346	18	300	0.1258E-05	0.078
317	5	6	135	3395	339	39	300	0.1257E-05	0.052
321	5	7	26	3436	296	- 6	300	0.9003E-06	0.041
325	6	1	141				300	0.1166E-04	0.187
							400	0.4557E-05	0.073
							450	0.2356E-05	0.038
340	6	3	116	3556	260	-47	300	0.9980E-06	0.040
							400	0.1341E-05	0.050
342	6	3	136	3576	164	29	300	0.2420E-05	0.083
							400	0.1561E-05	0.054
343	6	3	146	3586	205	-37	400	0.1929E-05	0.094
							500	0.1308E-05	0.063
							600	0.1188E-05	0.058
344	6	4	6	3596	210	-34	300	0.3350E-05	0.172
345	6	4	16	3606	219	-56	400	0.3452E-05	0.205
							500	0.2173E-05	0.129

Table 3. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	Demagnetization Level (OE)	J (emu)	J/J_0
347	6	4	36	3626	46	8	500	0.2490E-05	0.057
							600	0.2787E-05	0.064
							700	0.2872E-05	0.066
							800	0.2223E-05	0.051
349	6	4	56	3646	106	13	500	0.2871E-05	0.054
							600	0.2915E-05	0.055
							700	0.2339E-05	0.044
351	6	4	76	3666	47	49	300	0.4827E-05	0.184
353	6	4	96	3686	50	11	300	0.2240E-05	0.085
							400	0.2622E-05	0.100
							500	0.2168E-05	0.082
							600	0.1755E-05	0.067
355	6	4	116	3706	245	-50	300	0.1180E-05	0.045
357	6	4	136	3726			300	0.1233E-05	0.055
							400	0.1212E-05	0.054
							400	0.6656E-06	0.030
							500	0.9008E-06	0.040
373	6	5	146	3886	125	-13	300	0.1312E-05	0.059
							400	0.1856E-05	0.084
							500	0.3103E-05	0.141
							600	0.3332E-05	0.151
							800	0.3900E-05	0.177
							1000	0.4200E-05	0.190
							1000	0.4400E-05	0.199
376	6	6	26	3916			300	0.4524E-06	0.040
							300	0.7400E-06	0.066
							400	0.1510E-05	0.135
							400	0.5800E-06	0.052
377	6	6	36	3926	183	33	300	0.9439E-06	0.048
378	6	6	46	3936	216	-43	300	0.7285E-05	0.204
381	6	6	76	3966	245	-32	300	0.3289E-05	0.259
							400	0.4064E-05	0.321
							500	0.5379E-05	0.424
383	6	6	96	3986	299	48	300	0.3170E-05	0.141
							400	0.4420E-05	0.197
384	6	6	106	3996	290	27	300	0.3155E-05	0.101
385	6	6	116	4006	30	11	300	0.4908E-05	0.145
							400	0.2875E-05	0.085
388	6	6	146	4036	3	15	300	0.3472E-05	0.127
389	6	6	6	4046	255	12	300	0.5214E-05	0.197
							400	0.6814E-05	0.257
							500	0.7657E-05	0.289
							600	0.8285E-05	0.313
391	6	7	26	4066	306	27	300	0.5510E-05	0.233
							400	0.5310E-05	0.224
							500	0.6320E-05	0.267
							600	0.6830E-05	0.289
392	6	7	36	4076	347	34	300	0.6526E-05	0.208
							400	0.4423E-05	0.141
							500	0.5433E-05	0.173
							600	0.5203E-05	0.166
							800	0.5731E-05	0.182
							1000	0.6848E-05	0.218
393	6	7	44	4084	324	38	300	0.5410E-05	0.173
							400	0.5470E-05	0.175
							500	0.4140E-05	0.132
							600	0.5430E-05	0.173
							700	0.6590E-05	0.210

Table 3. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	Demagnetization Level (OE)	J (emu)	J/J_0
							800	0.7850E-05	0.251
							900	0.5600E-05	0.179
395	7	1	16	4476	295	-39	300	0.1054E-04	0.410
							400	0.4661E-05	0.181
							500	0.3836E-05	0.149
396	7	1	26	4486	357	-52	300	0.2593E-04	0.292
							400	0.1020E-04	0.115
							500	0.6990E-05	0.079
							600	0.4430E-05	0.050
							800	0.3700E-05	0.042
							1000	0.3980E-05	0.045
397	7	1	36	4496	167	-61	300	0.2738E-04	0.256
							400	0.1313E-04	0.123
							500	0.7683E-05	0.072
							600	0.4709E-05	0.044
398	7	1	46	4506	211	-45	300	0.4884E-04	0.240
							400	0.2141E-04	0.105
							500	0.1352E-04	0.066
							600	0.1124E-04	0.055
400	7	1	66	4526	130	-25	300	0.1252E-04	0.271
							400	0.5118E-05	0.111
405	7	1	116	4576	137	-20	300	0.3051E-05	0.170
							400	0.4553E-06	0.025
							400	0.6295E-06	0.035
							500	0.1274E-05	0.071
							500	0.1924E-05	0.107
408	7	1	146	4606	283	1	300	0.2743E-05	0.102
							400	0.3182E-05	0.118
							400	0.4367E-05	0.162
							500	0.3784E-05	0.140
							500	0.3832E-05	0.142
410	7	2	26				300	0.8580E-06	0.042
411	7	2	36				300	0.1439E-05	0.094
							400	0.2103E-05	0.138
415	7	2	86	4646	114	-25	300	0.8551E-05	0.211
421	7	2	146	4706	279	20	300	0.5011E-05	0.119
							400	0.3785E-05	0.090
422	7	3	5	4716	258	23	300	0.8281E-06	0.026
424	7	3	26	4736	242	12	150	0.2683E-05	0.076
							300	0.1263E-05	0.036
							300	0.1614E-05	0.046
							400	0.1120E-05	0.032
							400	0.9046E-06	0.026
425	7	3	36	4746	159	-23	300	0.1095E-05	0.062
							400	0.2421E-05	0.138
							400	0.3064E-05	0.174
							450	0.2350E-05	0.134
							500	0.2334E-05	0.133
426	7	3	46	4756	223	-18	300	0.2127E-05	0.088
							400	0.1170E-05	0.048
							500	0.2343E-05	0.097
							600	0.1267E-05	0.052
							600	0.1842E-05	0.076
427	7	3	56	4766	286	-23	400	0.1429E-05	0.074
							400	0.9473E-06	0.049
							500	0.1382E-05	0.071
							500	0.1553E-05	0.080
429	7	3	76	4786	272	25	300	0.2087E-05	0.074

Table 3. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	Demagnetization Level (OE)	J (emu)	J/J_0
							400	0.1667E-05	0.059
432	7	3	106	4816	305	-40	300	0.3527E-05	0.155
							400	0.1460E-05	0.064
							500	0.1589E-05	0.070
434	7	3	126	4836	283	31	300	0.1023E-04	0.143
436	7	3	146	4856	275	36	300	0.9860E-05	0.129
438	7	4	16	4876	266	34	300	0.1225E-04	0.139
440	7	4	36	4896	278	40	300	0.1338E-05	0.028
442	7	4	56	4916	251	49	300	0.7719E-06	0.021
444	7	4	76	4936	114	-24	300	0.5653E-05	0.181
446	7	4	96	4956	61	-25	300	0.1366E-05	0.046
							400	0.1862E-05	0.063
							500	0.3275E-05	0.110
							600	0.3413E-05	0.115
447	7	4	106	4966	71	-26	300	0.2589E-05	0.107
450	7	4	136	4996	62	17	300	0.6054E-06	0.017
							300	0.9025E-06	0.026
							400	0.1403E-05	0.040
							500	0.3012E-05	0.086
451	7	4	146	5006	91	-36	300	0.4135E-05	0.133
453	7	5	16	5026	115	-16	300	0.9808E-06	0.033
459	7	5	76	5086	229	27	300	0.2097E-05	0.067
							400	0.1594E-05	0.051
460	7	5	86	5096	242	34	300	0.2234E-05	0.058
461	7	5	96	5106	238	46	300	0.1666E-05	0.095
							400	0.2485E-05	0.142
							500	0.2982E-05	0.171
465	7	5	136	5146	79	-18	250	0.6459E-05	0.366
							300	0.4089E-05	0.232
466	7	5	146	5156	100	-40	300	0.1431E-05	0.053
							400	0.2179E-05	0.080
							400	0.6568E-06	0.024
							500	0.1013E-05	0.037
469	7	6	26	5186	119	-17	300	0.1176E-05	0.034
471	7	6	46	5206	102	8	250	0.1576E-05	0.049
							300	0.4906E-06	0.015
472	7	6	56	5216	94	-28	300	0.3531E-05	0.169
475	7	6	86	5246			300	0.1829E-05	0.053
							400	0.2760E-05	0.079
							500	0.2992E-05	0.086
477	7	6	106	5266	283	35	300	0.2785E-05	0.065
							400	0.2138E-05	0.050
479	7	6	126	5286	48	-19	300	0.1420E-05	0.040
480	7	6	136	5296	94	-29	300	0.3077E-05	0.143
							400	0.8370E-06	0.039
							500	0.2507E-05	0.116
481	7	6	146	5306	108	-15	300	0.1290E-04	0.374
							400	0.4970E-05	0.144
482	7	7	6	5316	100	-21	300	0.6480E-05	0.306
							400	0.2221E-05	0.105
483	7	7	16	5326	127	-26	300	0.1830E-05	0.048
							400	0.1830E-05	0.048
							400	0.2130E-05	0.056
484	7	7	26	5336	293	51	300	0.1230E-05	0.030
							300	0.9400E-06	0.023
485	7	7	36	5346	259	45	300	0.2310E-05	0.058
							400	0.1940E-05	0.049
							500	0.2960E-05	0.075

Table 3. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	Demagnetization Level (OE)	J (emu)	J/J_0
							600	0.2810E-05	0.071
							800	0.3370E-05	0.085
							1000	0.3340E-05	0.084
							1000	0.3510E-05	0.089
487	8	1	26	5436	146	-51	300	0.1048E-04	0.498
							400	0.3773E-05	0.179
							500	0.3590E-05	0.171
							500	0.3828E-05	0.182
							600	0.3740E-05	0.178
488	8	1	36	5446	118	-67	300	0.6513E-05	0.200
							400	0.4304E-05	0.132
							500	0.4006E-05	0.123
489	8	1	46	5456	143	-18	300	0.1440E-04	0.193
							400	0.7524E-05	0.101
							500	0.4269E-05	0.057
							600	0.3166E-05	0.043
490	8	1	56	5466	318	-53	300	0.5509E-05	0.193
							400	0.1884E-05	0.066
							500	0.2255E-05	0.079
491	8	1	66	5476	312	-41	300	0.5083E-05	0.162
494	8	1	96	5506	190	1	300	0.2642E-05	0.030
							300	0.2751E-05	0.032
495	8	1	106	5516	327	-13	300	0.9768E-05	0.298
498	8	1	136	5546	190	- 3	300	0.4784E-05	0.073
							400	0.1724E-05	0.026
499	8	1	146	5556	321	-20	300	0.9775E-05	0.327
500	8	2	5	5565	137	15	300	0.2161E-04	0.222
							400	0.1064E-04	0.109
							500	0.4788E-05	0.049
							500	0.4807E-05	0.049
502	8	2	32	5592	141	17	300	0.1069E-04	0.142
							400	0.6719E-05	0.089
							500	0.2200E-05	0.029
503	8	2	67	5627	178	49	300	0.2262E-05	0.046
505	8	2	106	5666	140	19	300	0.1180E-04	0.164
507	8	2	126	5686	292	- 9	300	0.3371E-05	0.062
							400	0.1210E-05	0.022
509	8	2	146	5706	304	54	300	0.1592E-05	0.041
							400	0.8995E-06	0.023
511	8	3	66	5776	123	-20	300	0.1494E-05	0.039
513	8	3	101	5811	146	18	250	0.2269E-05	0.044
							300	0.1811E-05	0.035
514	8	3	147	5857	311	-14	300	0.4948E-05	0.158
							400	0.1063E-05	0.034
515	8	4	3	5863	132	-18	300	0.6623E-05	0.340
							400	0.2348E-05	0.121
517	8	4	23	5883	114	9	300	0.3409E-05	0.137
							400	0.2093E-05	0.084
521	8	6	77	6237			300	0.2245E-04	1.029
							400	0.9355E-05	0.429
							500	0.4326E-05	0.198
							500	0.4334E-05	0.199
522	8	6	90	6250	345	-14	300	0.2051E-04	0.643
							400	0.8676E-05	0.272
523	8	7	39	6349	157	-12	300	0.9922E-06	0.044

Table 4. Magnetization of Hole 576B samples after AF demagnetization at intensities above 100 Oe.

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Demagnetization Level (OE)	J (emu)	J/J_0
617	1	5	6	606	300	0.1255E-04	0.555
624	1	5	76	676	201	0.1309E-04	0.668
625	1	5	86	686	300	0.6085E-05	0.861
				686	301	0.4694E-05	0.664
				686	400	0.4220E-05	0.597
				686	500	0.3285E-05	0.465
				686	600	0.2845E-05	0.402
611	1	6	6	756	300	0.9197E-05	0.739
632	2	1	11	1171	201	0.9128E-05	0.846
635	2	1	36	1196	201	0.1590E-04	0.747
685	2	5	16	1776	300	0.3081E-05	0.831
688	2	5	46	1806	300	0.8236E-05	0.608
707	2	6	86	1996	201	0.4483E-05	1.257
711	2	6	126	2036	202	0.5460E-06	0.073
				2036	300	0.5960E-06	0.080
713	2	6	146	2056	300	0.4284E-06	0.073
714	2	7	6	2066	201	0.6357E-05	0.596
				2066	300	0.4061E-05	0.381
				2066	400	0.2057E-05	0.193
				2066	500	0.1327E-05	0.125
				2066	600	0.1174E-05	0.110
716	2	7	26	2086	300	0.4193E-05	0.294
				2086	301	0.5282E-05	0.371
				2086	400	0.2936E-05	0.206
				2086	500	0.1678E-05	0.118
				2086	600	0.1240E-05	0.087
				2086	700	0.7874E-06	0.055
752	3	3	46	2326	300	0.2409E-05	0.249
				2326	400	0.1547E-05	0.160
770	3	6	126	2552	300	0.6193E-06	0.039
				2552	400	0.3523E-06	0.022
775	4	3	106	3416	300	0.1801E-05	0.122
				3416	400	0.9116E-06	0.062
776	4	3	126	3436	300	0.1672E-05	0.189
777	4	3	146	3456	300	0.4622E-06	0.034
778	4	4	6	3466	300	0.1027E-05	0.060
779	4	4	26	3486	300	0.7908E-06	0.055
780	4	4	46	3506	300	0.7645E-06	0.050
781	4	4	66	3526	300	0.7230E-06	0.060
782	4	4	86	3546	300	0.7836E-06	0.064
783	4	4	106	3566	300	0.8954E-06	0.062
785	4	4	146	3606	300	0.7728E-06	0.052
786	4	5	6	3616	300	0.1445E-05	0.099
				3615	401	0.6454E-06	0.044
787	4	5	26	3636	300	0.6849E-06	0.045
788	4	5	46	3656	300	0.8751E-06	0.043
789	4	5	66	3676	300	0.9333E-06	0.058
790	4	5	86	3696	300	0.1566E-05	0.095
791	4	5	106	3716	300	0.2116E-05	0.133
792	4	5	126	3736	300	0.1622E-05	0.000
				3736	400	0.9335E-06	0.000
793	4	5	146	3756	300	0.1806E-05	0.179
				3756	400	0.8306E-06	0.082
794	4	6	6	3766	300	0.1663E-05	0.159
795	4	6	26	3786	300	0.1433E-05	0.165
796	4	6	46	3806	300	0.2593E-05	0.311
				3806	400	0.1095E-05	0.132
800	4	6	126	3886	300	0.3337E-05	0.268

Table 4. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Demagnetization Level (OE)	J (emu)	J/J_0
801	4	6	146	3906	300	0.5924E-05	0.183
				3906	400	0.3753E-05	0.116
				3906	500	0.3010E-05	0.093
				3906	600	0.3041E-05	0.094
				3906	700	0.2625E-05	0.081
806	5	2	6	4016	300	0.3072E-05	0.188
809	5	2	67	4077	300	0.1872E-05	0.080
810	5	2	87	4097	300	0.1948E-05	0.086
817	5	3	66	4226	300	0.7327E-06	0.041
				4226	301	0.1094E-05	0.061
818	5	3	86	4246	300	0.2446E-05	0.151
820	5	3	126	4286	201	0.5567E-05	0.345
821	5	3	146	4306	201	0.1076E-04	0.688
835	5	5	107	4567	300	0.5734E-05	0.116
836	5	5	126	4586	300	0.3053E-05	0.241
				4586	400	0.4037E-05	0.318
838	5	6	6	4616	300	0.7755E-05	0.512
839	5	6	26	4636	300	0.9557E-05	0.528
850	6	2	86	5242	300	0.1668E-05	0.045
852	6	2	126	5282	300	0.1843E-05	0.048
				5282	400	0.1406E-05	0.037
865	6	4	66	5512	300	0.1478E-05	0.039
874	6	6	47	5793	300	0.3731E-05	0.091
				5793	400	0.2211E-05	0.054
				5793	500	0.2332E-05	0.057
893	8	5	142	7487	300	0.3206E-05	0.273
894	8	6	44	7539	300	0.5708E-05	0.423

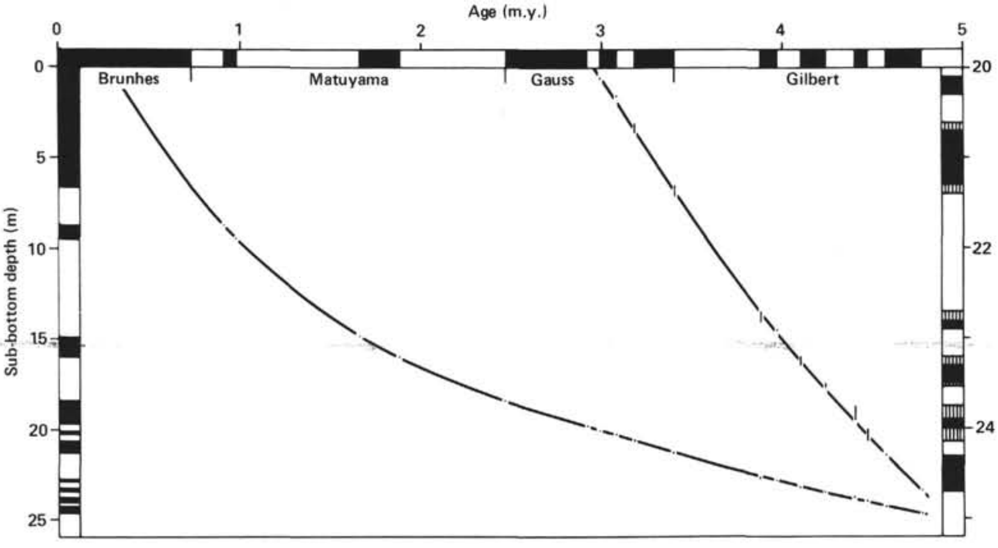

Figure 2. Correlation of the paleomagnetic polarity stratigraphy of Site 576 with the time scale of Berggren et al. (in press). The Gauss–Gilbert interval is replotted at an enlarged vertical scale (right-hand curve and depth scale; partly filled bars show intervals of uncertain polarity).

Table 5. Magnetostratigraphy for Site 576.

Age[a] (m.y.)	Depth (m) Hole 576	Hole 576B	Boundary or event
0.73	6.61 ± 0.05	6.61 ± 0.04	Brunhes/Matuyama
0.91	8.76 ± 0.04	—	Jaramillo
0.98	9.51 ± 0.09	—	
1.66	14.91 ± 0.04	14.91 ± 0.04	Olduvai
1.88	16.01 ± 0.04	—	
2.47	—	18.41 ± 0.04	Matuyama/Gauss
2.92	19.81 ± 0.04	19.91 ± 0.04	Kaena
2.99	20.11 ± 0.04	20.11 ± 0.04	
3.08	20.31 ± 0.04	20.31 ± 0.04	Mammoth
3.18	20.71 ± 0.04	20.61 ± 0.04	
3.40	21.41 ± 0.04	21.31 ± 0.04	Gauss/Gilbert
3.88	22.71 ± 0.04	22.81 ± 0.04	Cochiti
3.97	22.91 ± 0.04	22.91 ± 0.04	
4.10	23.31 ± 0.04	—	Nunivak
4.24	23.51 ± 0.04	—	
4.40	23.91 ± 0.04	—	Sidufjall
4.47	24.01 ± 0.04	—	
4.57	24.31 ± 0.04	—	Thvera
4.77	24.71 ± 0.04	24.61 ± 0.04	

Note: — means not recovered.
[a] From Berggren et al. (in press).

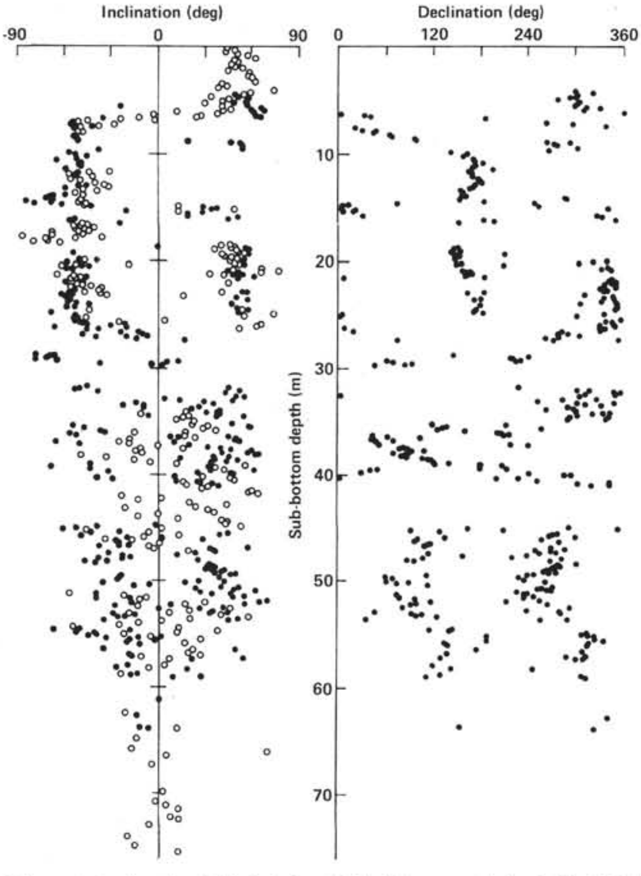

Figure 3. Inclination (filled circles, Hole 576; open circles, Hole 576B) and declination (Hole 576 only) of magnetic samples as a function of depth at Site 576.

tories at the two sites from the middle Miocene through the Pliocene (Fig. 11).

Prior to 16 m.y. ago at Site 578 and 5 m.y. at Site 576, the age-depth curves are constrained only by ichthyolith (see Doyle and Riedel, this volume) and limited foraminiferal (see D'Agostino, this volume) stratigraphy. The uncertainties in age assignments and relatively wide spacings of the control points conceal any short-term rate changes (i.e., <5-10 m.y.).

Within the uncertainties of the initial ichthyolith stratigraphies, the accumulation rates at the two sites from 16 to 70 m.y. ago are identical and uniform at about 0.4 m/m.y.

From about 16 to 2 m.y. ago, sediment accumulated at Site 578 about five times as fast as at Site 576. The process responsible for this difference has not been identified, but the sharpness of the isopach gradient near Site 578 (see Jacobi et al., this volume) suggests that transport by bottom currents to this site, rather than introduction of excess sediment at the sea surface, is a likely explanation.

CONCLUSIONS

Sites 576 and 578 both appear to contain essentially complete Cenozoic sections of pelagic clay. At Site 576, the accumulation rate increases gradually from about 0.4 m/m.y. prior to 15 m.y. ago to about 4 m/m.y. at 2 m.y. ago. An influx of Pleistocene eolian debris then results in a rapid increase to a rate in excess of 15 m/m.y. today. Stable detrital remanence yields a good paleomagnetic record for the past 5 m.y., during which period the accumulation rate has exceeded 2 m/m.y.

At Site 578, the accumulation rate prior to 16 m.y. ago was 0.3-0.4 m/m.y. It then increased abruptly to 2-4 m/m.y. for the interval from 16 to 9 m.y. ago. Following a hiatus from 8.2 to 8.8 m.y. ago, the rate increased fairly uniformly to the surface, reaching a maximum value of about 38 m/m.y. The rate increase during the Quaternary is very similar to the pattern at Site 576.

Site 578 contains a remarkable record of detrital remanence spanning the past 16 m.y. About 60 reversals can be correlated to the standard paleomagnetic stratigraphic section, yielding a detailed age-depth curve for the site. As at Site 576, the magnetic stratigraphy breaks down when the accumulation rate drops below about 2 m/m.y., owing, apparently, to "swamping" of the detrital remanence by the unstable chemical remanence of authigenic oxyhydroxides.

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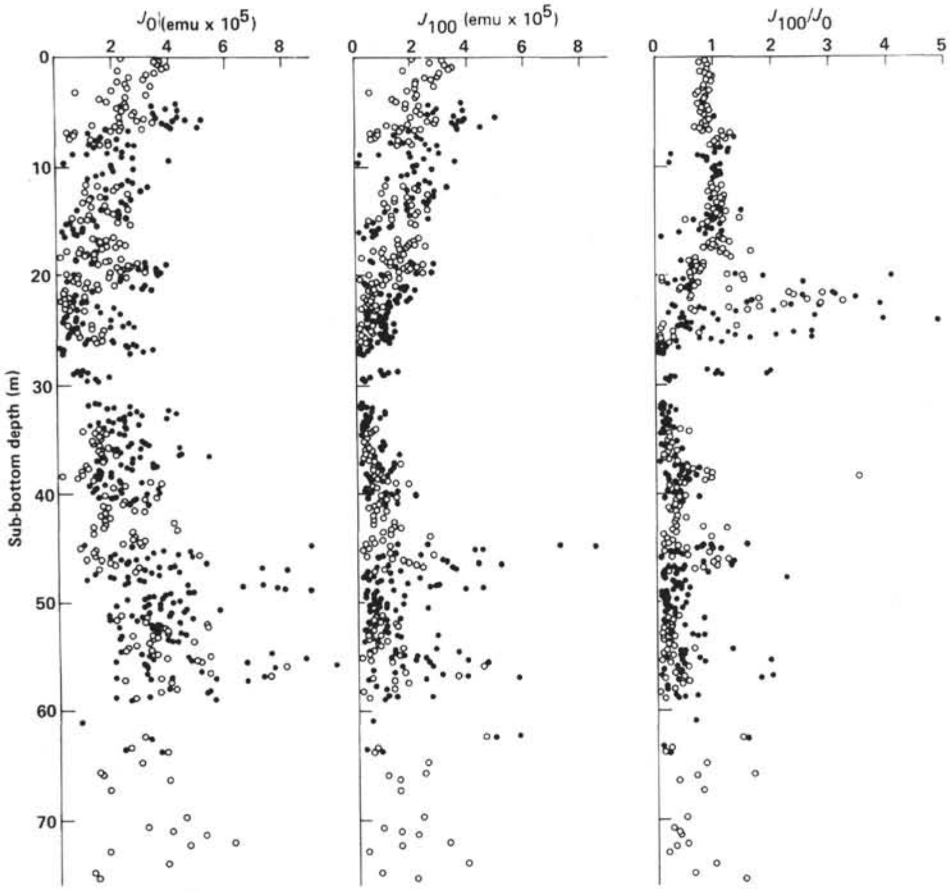

Figure 4. Natural remanent magnetization (J_0), remanent intensity after AF demagnetization at 100 Oe (J_{100}), and J_{100}/J_0 for samples from Site 576. Filled circles, Hole 576; open circles, Hole 576B.

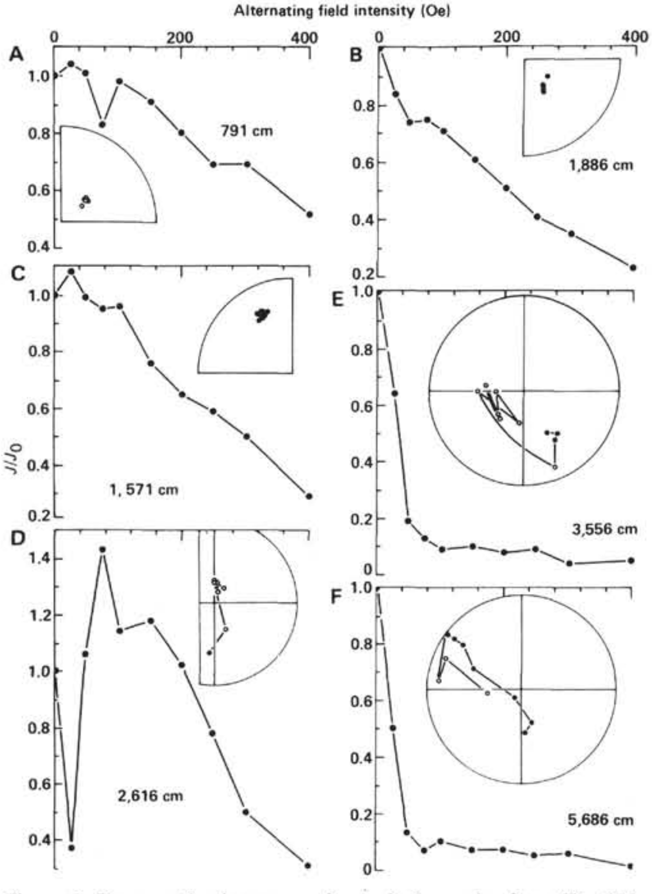

Figure 5. Demagnetization curves for typical samples from Site 576. (A) Sample 576-2-1, 96 cm, (B) Sample 576-4-1, 106 cm and (C) Sample 576-2-6, 126 cm yield stable estimates of detrital remanence, whereas (D) Sample 576-4-6, 86 cm, (E) Sample 576-6-3, 116 cm, and (F) Sample 576-8-2, 126 cm from the dark brown manganese-rich clays do not yield reliable detrital remanence values.

Table 6. Magnetic properties of samples from Site 578.

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	Note
901	1	1	16	16	173	47	0.9823E-04	0.8813E-04	0.897	L1
903	1	1	53	53	150	53	0.8811E-04	0.7592E-04	0.862	L1
905	1	1	86	86	116	44	0.1419E-04	0.1039E-04	0.732	L1
906	1	1	106	106	96	52	0.4563E-04	0.3943E-04	0.864	L1
907	1	1	126	126			0.5234E-04			
908	1	1	146	146	91	55	0.6319E-04	0.5353E-04	0.847	L1
909	1	2	6	156	97	55	0.5295E-04	0.4980E-04	0.940	L1
911	1	2	50	200	79	50	0.5279E-04	0.3896E-04	0.738	L1
913	1	2	86	236	96	55	0.2965E-04	0.2809E-04	0.948	L1
915	1	2	126	276	112	64	0.4481E-04	0.3993E-04	0.891	L1
916	1	2	146	296	82	54	0.4955E-04	0.3969E-04	0.801	L1
917	1	3	6	306	117	48		0.5108E-04		L1
918	1	3	27	327	136	47	0.7817E-04	0.6858E-04	0.877	L1
919	1	3	46	346	126	51		0.7448E-04		L1
920	1	3	66	366	130	30	0.5894E-04	0.4499E-04	0.763	L1
921	1	3	86	386	149	41	0.5645E-04	0.4376E-04	0.775	L1
923	1	3	126	426	153	44	0.6618E-04	0.5542E-04	0.837	L1
925	2	1	6	486	201	40	0.6386E-04	0.5296E-04	0.829	L1
927	2	1	43	523	219	56	0.5751E-04	0.4656E-04	0.810	L1
929	2	1	86	566	218	30	0.3148E-04	0.2548E-04	0.809	L1
931	2	1	126	606	251	62	0.5760E-04	0.5276E-04	0.916	L1
932	2	1	146	626	232	48	0.5948E-04	0.5291E-04	0.890	L1
933	2	2	5	635	232	-28	0.3430E-04	0.2636E-04	0.768	L1
934	2	2	26	656	237	42	0.5290E-04	0.4363E-04	0.825	L1
935	2	2	46	676	222	54	0.4485E-04	0.3730E-04	0.832	L1
937	2	2	86	716	242	54	0.5689E-04	0.4919E-04	0.865	L1
939	2	2	126	756	235	64	0.5176E-04	0.4532E-04	0.876	L1
941	2	3	16	796	243	37	0.2839E-04	0.2359E-04	0.831	L1,F
942	2	3	41	821	234	48	0.1158E-03	0.8305E-04	0.717	L1
943	2	3	66	846	189	19	0.6138E-04	0.5086E-04	0.829	L1
944	2	3	86	866	176	55	0.5493E-04	0.4996E-04	0.909	L1
945	2	3	106	886	178	51	0.6649E-04	0.5105E-04	0.768	L1
947	2	3	144	924	172	54	0.4597E-04	0.3624E-04	0.788	L1
949	2	4	26	956	167	59	0.8649E-04	0.7093E-04	0.820	L1
951	2	4	64	994	159	61	0.8073E-04	0.6583E-04	0.815	L1
953	2	4	106	1036	174	49	0.5319E-04	0.4363E-04	0.820	L1
955	2	4	146	1076	178	49	0.5833E-05	0.4645E-05	0.796	L1
957	2	5	26	1106	177	59	0.6167E-04	0.5225E-04	0.847	L1
959	2	5	66	1146	187	60	0.7992E-04	0.6815E-04	0.853	L1
961	2	5	106	1186	180	59	0.8308E-04	0.6693E-04	0.806	L1
963	2	6	6	1236	186	55	0.9513E-04	0.7451E-04	0.783	L1
965	3	1	4	1434	351	45	0.1195E-03	0.9947E-04	0.832	L1
967	3	1	46	1476	3	64	0.8910E-05	0.7434E-05	0.834	L1
969	3	1	86	1516	355	54	0.2057E-04	0.1716E-04	0.834	L1
970	3	1	106	1536	5	53	0.4809E-04	0.4028E-04	0.838	L1
971	3	1	126	1556	5	-58	0.3841E-04	0.3398E-04	0.885	L1
972	3	1	146	1576	357	47	0.4986E-04	0.4115E-04	0.825	L1
973	3	2	6	1586	9	55	0.4534E-04	0.3737E-04	0.824	L1
975	3	2	46	1626	358	51	0.2706E-04	0.2394E-04	0.885	L1
977	3	2	86	1666	8	60	0.6184E-04	0.5196E-04	0.840	L1
979	3	2	126	1706	18	58	0.5784E-04	0.4808E-04	0.831	L1
980	3	2	146	1726	23	54	0.5837E-04	0.4957E-04	0.849	L1
981	3	3	6	1736	52	-13	0.5258E-04	0.4256E-04	0.809	L1
982	3	3	26	1756	15	53	0.8643E-04	0.7252E-04	0.839	L1
983	3	3	46	1776	28	55	0.5266E-04	0.4174E-04	0.793	L1
985	3	3	83	1813	22	56	0.6009E-04	0.5335E-04	0.888	L1
987	3	3	126	1856	38	54	0.7511E-04	0.6474E-04	0.862	L1
989	3	4	6	1886	34	52	0.6767E-04	0.5842E-04	0.863	L1
991	3	4	46	1926	44	54	0.5153E-04	0.4372E-04	0.848	L1
993	3	4	86	1966	43	54	0.5618E-04	0.5377E-04	0.957	L1

Table 6. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	Note
995	3	4	126	2006	49	57	0.7995E-04	0.7084E-04	0.886	L1
997	3	5	6	2036	50	48	0.9282E-04	0.8056E-04	0.868	L1
999	3	5	46	2076	48	54	0.7261E-04	0.6503E-04	0.896	L1
1001	3	5	86	2116	58	58	0.7631E-04	0.6187E-04	0.811	L1
1003	3	5	126	2156	67	52	0.1058E-03	0.9329E-04	0.882	L1
1005	3	6	6	2186	79	48	0.4716E-04	0.3893E-04	0.825	L1
1007	3	6	50	2230	79	66	0.8473E-05	0.6610E-05	0.780	L1
1009	3	6	86	2266	63	56	0.2053E-05	0.1705E-05	0.830	L1
1011	3	7	6	2336	67	49	0.4198E-04	0.3244E-04	0.773	L1
1013	3	7	46	2376	66	53	0.3954E-04	0.3326E-04	0.841	L1
1015	4	1	26	2406	333	75	0.9327E-05	0.7909E-05	0.848	L1
1017	4	1	66	2446	329	47	0.4799E-04	0.4128E-04	0.860	L1
1019	4	1	113	2493	340	47	0.4362E-04	0.3854E-04	0.883	L1
1021	4	1	145	2525	329	53	0.4006E-04	0.3469E-04	0.866	L1
1023	4	2	25	2555	328	46	0.4658E-04	0.3951E-04	0.848	L1
1025	4	2	66	2596	321	51	0.6295E-04	0.5487E-04	0.872	L1
1027	4	2	108	2638	329	58	0.6493E-04	0.5450E-04	0.839	L1
1029	4	2	146	2676	332	56	0.5844E-04	0.5307E-04	0.908	L1
1039	4	3	26	2706	312	50	0.4358E-04	0.3634E-04	0.834	L1
1041	4	3	66	2746	314	29	0.7841E-04	0.6466E-04	0.825	L1
1042	4	3	86	2766	266	49	0.4281E-04	0.3593E-04	0.839	L1
1043	4	3	105	2785	116	-12	0.6468E-05	0.8880E-05	1.373	A2-3
1031	4	4	25	2855	99	-58	0.4112E-04	0.4355E-04	1.059	L1
1033	4	4	65	2895	65	-29	0.5159E-06	0.6415E-06	1.243	L1
1035	4	4	110	2940	65	-50	0.9491E-06	0.9051E-06	0.954	A3-4
1037	4	4	146	2976	68	-52	0.6026E-05	0.5643E-05	0.937	L1
1044	4	3	126	2806	95	-61	0.3614E-04	0.3452E-04	0.955	L1
1045	4	3	146	2826	79	-52	0.5822E-04	0.6056E-04	1.040	L1
1047	4	5	32	3012	50	-50	0.2102E-04	0.2156E-04	1.026	L1
1049	4	5	66	3046	49	-46	0.9623E-05	0.9706E-05	1.009	L1
1051	4	5	106	3086	41	-59	0.1535E-04	0.1903E-04	1.240	L1
1053	4	5	146	3126	22	-54	0.4646E-04	0.5007E-04	1.078	L1
1055	4	6	26	3156	10	-55	0.3728E-04	0.4142E-04	1.111	L1
1056	4	6	46	3176	10	-51	0.3980E-04	0.4380E-04	1.101	L1
1057	4	6	66	3196	2	57	0.2730E-04	0.3323E-04	1.217	L1
1059	4	6	114	3244	161	56	0.5555E-04	0.4381E-04	0.789	L1
1061	5	1	47	3377	330	48	0.5012E-04	0.4458E-04	0.889	L1
1062	5	1	106	3436	2	67	0.1931E-04	0.1509E-04	0.781	L1
1063	5	1	126	3456	154	-57	0.3798E-04	0.3878E-04	1.021	L1
1065	5	2	6	3486	162	-47	0.6264E-04	0.5965E-04	0.952	L1
1067	5	2	51	3531	156	-42	0.4311E-04	0.4515E-04	1.047	L1
1069	5	2	85	3565	143	-39	0.1035E-04	0.1277E-04	1.234	L1
1071	5	2	126	3606	167	-49	0.5329E-04	0.5386E-04	1.011	L1
1073	5	3	6	3636	165	-49	0.6879E-04	0.6906E-04	1.004	L1
1075	5	3	45	3675	168	-51	0.4353E-04	0.4475E-04	1.028	L1
1077	5	3	86	3716	167	-52	0.3510E-04	0.3907E-04	1.113	L1
1078	5	3	105	3735	178	-44	0.1619E-04	0.1990E-04	1.230	L1
1079	5	3	128	3758	356	44	0.2183E-04	0.1661E-04	0.761	L1
1080	5	3	146	3776	46	-45	0.4044E-04	0.4543E-05	0.112	L1
1081	5	4	6	3786	167	-38	0.1102E-04	0.1270E-04	1.153	L1
1083	5	4	46	3826	176	-46	0.3321E-04	0.3177E-04	0.957	L1
1085	5	4	86	3866	174	-48	0.3601E-04	0.3666E-04	1.018	L1
1087	5	4	126	3906	181	-52	0.1873E-04	0.1999E-04	1.067	L1
1089	5	5	6	3936	151	-52	0.6993E-06	0.5485E-06	0.784	L1
1091	5	5	46	3976	184	-54	0.9561E-05	0.8065E-05	0.844	L1
1093	5	5	86	4016	197	-52	0.2632E-04	0.2318E-04	0.881	L1
1095	5	5	128	4058	175	-51	0.1753E-04	0.1544E-04	0.881	L1
1097	5	6	6	4086	188	-52	0.2485E-04	0.2129E-04	0.857	L1
1099	5	6	46	4126	177	-52	0.6102E-04	0.5938E-04	0.973	L1
1101	5	6	86	4166	191	-54	0.7963E-04	0.7240E-04	0.909	L1

Table 6. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	Note
1103	5	6	126	4206	194	-55	0.7699E-04	0.7254E-04	0.942	L1
1105	5	7	22	4252	190	-56	0.4073E-04	0.3743E-04	0.919	L1
1107	6	1	6	4286			0.4570E-05	0.2415E-05	0.529	F
1109	6	1	67	4347	31	-51	0.3309E-04	0.3485E-04	1.053	L1
1111	6	1	106	4386	43	-57	0.4049E-04	0.3598E-04	0.889	L1
1113	6	1	146	4426	63	-56	0.1237E-04	0.1056E-04	0.854	L1
1115	6	2	26	4456	35	-48	0.3326E-04	0.3226E-04	0.970	L1
1117	6	2	66	4496	53	-51	0.3450E-04	0.3643E-04	1.056	L1
1119	6	2	106	4536	56	-41	0.5831E-04	0.5671E-04	0.972	L1
1121	6	2	146	4576	71	-46	0.7053E-04	0.7330E-04	1.039	L1
1123	6	3	26	4606	66	-55	0.5079E-04	0.4799E-04	0.945	L1
1125	6	3	63	4643	81	-54	0.7311E-04	0.7222E-04	0.988	L1
1127	6	3	102	4682	88	-53	0.3394E-04	0.3314E-04	0.976	L1
1129	6	3	146	4726	63	-57	0.6839E-06	0.6920E-06	1.012	L1
1131	6	4	24	4756	81	-48	0.2404E-05	0.2218E-05	0.923	L1
1133	6	4	66	4796	86	-52	0.1841E-04	0.1699E-04	0.923	L1
1135	6	4	106	4836	83	-51	0.2761E-04	0.2668E-04	0.966	L1
1137	6	4	146	4876	99	-55	0.2893E-04	0.3367E-04	1.164	L1
1139	6	5	26	4906	90	-55	0.6737E-04	0.6803E-04	1.010	L1
1141	6	5	66	4946	68	-59	0.3964E-04	0.4335E-04	1.094	L1
1143	6	5	106	4986	67	-52	0.2143E-04	0.2457E-04	1.146	L1
1145	6	5	146	5026	79	-49	0.2629E-04	0.2353E-04	0.895	L1
1147	6	6	34	5064	72	-37	0.1374E-05	0.1244E-05	0.906	L1
1149	6	6	86	5116	75	-50	0.2321E-04	0.2111E-04	0.910	L1
1151	6	7	3	5183	73	-56	0.4278E-04	0.4016E-04	0.939	L1
1153	6	7	43	5223	70	-57	0.2653E-04	0.2431E-04	0.916	L1
1155	7	1	46	5266	301	-38	0.3578E-04	0.3165E-04	0.884	L1
1157	7	1	86	5306	298	-60	0.7281E-04	0.6341E-04	0.871	L1
1159	7	1	126	5346	298	-61	0.1145E-04	0.1157E-04	1.011	L1
1160	7	1	146	5366	122	50	0.3663E-04	0.3182E-04	0.869	L1
1161	7	2	6	5376	123	58	0.3285E-04	0.2974E-04	0.905	L1
1162	7	2	28	5398	263	-44	0.1595E-04	0.1418E-04	0.889	L1
1163	7	2	46	5416	114	47	0.3948E-04	0.3696E-04	0.936	L1
1165	7	2	86	5456	133	47	0.6829E-04	0.5882E-04	0.861	L1
1167	7	2	131	5501	122	49	0.5317E-04	0.4489E-04	0.844	L1
1169	7	3	6	5526	116	46	0.4255E-04	0.3519E-04	0.827	L1
1171	7	3	46	5566	129	46	0.4265E-04	0.3646E-04	0.855	L1
1173	7	3	86	5606	122	58	0.6792E-04	0.6968E-04	1.026	L1
1175	7	3	126	5646	125	58	0.6372E-04	0.5330E-04	0.836	L1
1177	7	4	6	5676	143	57	0.8232E-04	0.7665E-04	0.931	L1
1179	7	4	26	5717	140	52	0.5154E-04	0.4050E-04	0.786	L1
1181	7	4	86	5756	148	58	0.8095E-04	0.7638E-04	0.944	L1
1183	7	4	126	5796	160	50	0.2698E-04	0.2158E-04	0.800	L1
1184	7	4	146	5816	325	-56	0.2340E-04	0.2715E-04	1.160	L1
1185	7	5	6	5826	328	-55	0.3487E-04	0.3819E-04	1.095	L1
1187	7	5	46	5866	316	-78	0.1187E-04	0.1923E-04	1.619	L1
1189	7	5	66	5906	321	-49	0.6215E-04	0.6744E-04	1.085	L1
1191	7	5	126	5946	312	-56	0.6257E-04	0.6426E-04	1.027	L1
1193	7	6	6	5976	306	-46	0.4563E-04	0.4633E-04	1.015	L1
1195	7	6	45	6015	315	-48	0.5123E-04	0.5166E-04	1.008	L1
1197	7	6	86	6056	323	-47	0.4669E-04	0.5263E-04	1.127	L1
1199	7	6	126	6096	308	-50	0.4198E-04	0.4282E-04	1.020	L1
1201	7	7	11	6131	304	-58	0.5380E-04	0.5343E-04	0.993	L1
1202	7	7	46	6166	295	-59	0.4657E-04	0.4697E-04	1.009	L1
1203	8	1	26	6206	165	54	0.1504E-04	0.1333E-04	0.886	L1
1204	8	1	46	6226	315	-62	0.1115E-05	0.1064E-05	0.954	L1
1205	8	1	66	6246	272	42	0.1202E-04	0.1035E-04	0.861	L1
1206	8	1	87	6267	75	-59	0.7472E-06	0.6568E-06	0.879	L1
1207	8	1	92	6272	92	-50	0.1924E-05	0.1868E-05	0.971	L1
1209	8	1	126	6306	81	-53	0.1483E-05	0.1404E-05	0.947	L1

Table 6. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	Note
1211	8	2	6	6336	73	-45	0.2489E-05	0.2406E-05	0.967	L1
1213	8	2	46	6376	61	-51	0.4387E-04	0.3952E-04	0.901	L1
1215	8	2	86	6416	64	-49	0.6411E-04	0.5885E-04	0.918	L1
1217	8	2	126	6456	54	-55	0.6024E-04	0.5416E-04	0.899	L1
1219	8	3	6	6486	68	-56	0.6618E-04	0.6401E-04	0.967	L1
1221	8	3	46	6526	64	-56	0.7144E-04	0.6561E-04	0.918	L1
1223	8	3	86	6566	65	-50	0.5553E-04	0.5890E-04	1.061	L1
1225	8	3	126	6606	65	-46	0.4465E-04	0.4530E-04	1.014	L1
1227	8	4	6	6636	48	-43	0.4288E-04	0.4636E-04	1.081	L1
1229	8	4	48	6678	52	-51	0.6347E-04	0.6089E-04	0.959	L1
1231	8	4	86	6716	59	-34	0.4446E-04	0.4295E-04	0.966	L1
1233	8	4	126	6756	64	-44	0.4565E-04	0.4579E-04	1.003	L1
1235	8	5	6	6786	61	-41	0.4855E-04	0.4737E-04	0.976	L1
1237	8	5	46	6826	70	-43	0.4080E-04	0.4001E-04	0.981	L1
1239	8	5	86	6866	73	-45	0.1511E-04	0.1806E-04	1.195	L1
1241	8	5	123	6903	78	-50	0.5791E-04	0.6302E-04	1.088	L1
1243	8	6	6	6936	82	-49	0.3933E-04	0.4270E-04	1.086	L1
1245	8	6	46	6976	73	-56	0.1046E-03	0.1023E-03	0.977	L1
1247	8	6	91	7021	83	-60	0.7549E-04	0.7968E-04	1.056	L1
1249	8	6	126	7056	75	-47	0.6629E-04	0.6296E-04	0.950	L1
1251	8	7	5	7085	75	-49	0.8053E-04	0.7936E-04	0.985	L1
1253	8	7	36	7116	88	-55	0.8628E-04	0.9006E-04	1.044	L1
1255	9	1	31	7161	77	-43	0.1602E-04	0.1723E-04	1.076	L1
1257	9	1	66	7196	61	-56	0.4017E-04	0.4508E-04	1.122	L1
1258	9	1	86	7216	67	32	0.5689E-04	0.6237E-04	1.096	L1
1259	9	1	106	7236	71	-42	0.6136E-04	0.6231E-04	1.015	L1
1260	9	1	126	7256	58	-45	0.1512E-04	0.1930E-04	1.276	L1
1261	9	2	146	7276	249	50	0.4425E-04	0.3795E-04	0.858	L1
1263	9	2	26	7306	61	48	0.7538E-04	0.7155E-04	0.949	L1
1265	9	2	67	7347	49	55	0.6244E-04	0.5327E-04	0.853	L1
1267	9	2	106	7386	78	61	0.3821E-04	0.3532E-04	0.924	L1
1269	9	2	146	7426	61	49	0.1010E-03	0.8029E-04	0.795	L1
1271	9	3	26	7456	112	42	0.8663E-04	0.8172E-04	0.943	L1
1273	9	3	66	7496	99	49	0.4996E-04	0.4038E-04	0.808	L1
1275	9	3	106	7536	104	37	0.6787E-04	0.6201E-04	0.914	L1
1277	9	3	146	7576	117	45	0.1579E-04	0.1211E-04	0.767	L1
1279	9	4	26	7606	297	50	0.1086E-03	0.1057E-03	0.974	L1
1281	9	4	66	7646	312	41	0.7633E-04	0.6769E-04	0.887	L1
1283	9	4	106	7686	313	48	0.6943E-04	0.5788E-04	0.834	L1
1285	9	4	146	7726	314	50	0.5620E-04	0.4888E-04	0.870	L1
1287	9	5	25	7755	327	53	0.1161E-03	0.1040E-03	0.895	L1
1289	9	5	66	7796	322	57	0.7050E-04	0.5330E-04	0.756	L1
1291	9	5	100	7830	334	51	0.8589E-04	0.7122E-04	0.829	L1
1293	9	6	6	7886	316	47	0.6791E-04	0.6092E-04	0.897	L1
1295	9	6	46	7926	315	54	0.5598E-04	0.5325E-04	0.951	L1
1297	9	6	86	7966	325	54	0.5560E-04	0.4729E-04	0.851	L1
1299	9	6	126	8006	340	48	0.8341E-04	0.7401E-04	0.887	L1
1301	9	7	6	8036	336	50	0.8154E-04	0.7387E-04	0.906	L1
1302	9	7	26	8056	305	59	0.1581E-04	0.1061E-04	0.671	L1
1303	9	7	48	8078	141	-42	0.1182E-04	0.1174E-04	0.993	L1
1304	10	1	28	8108	31	55	0.4943E-04	0.4307E-04	0.871	L1
1305	10	1	46	8126	34	38	0.3978E-04	0.3666E-04	0.922	L1
1306	10	1	78	8158	235	-46	0.6801E-04	0.7009E-04	1.031	L1
1307	10	1	96	8176	221	-37	0.2774E-04	0.3139E-04	1.131	L1
1309	10	1	130	8210	223	-45	0.5719E-04	0.6044E-04	1.057	L1
1310	10	1	146	8226	217	-49	0.5144E-04	0.5110E-04	0.993	L1
1311	10	2	6	8236	196	-43	0.3538E-04	0.3561E-04	1.007	L1
1312	10	2	24	8254	11	48	0.4338E-04	0.3761E-04	0.867	L1
1313	10	2	46	8276	11	45	0.8454E-04	0.6420E-04	0.759	L1
1315	10	2	86	8316	8	52	0.7406E-04	0.6796E-04	0.918	L1

Table 6. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	Note
1317	10	2	126	8356	19	50	0.4981E-04	0.4010E-04	0.805	L1
1318	10	2	146	8376	183	-53	0.1745E-04	0.2662E-04	1.525	L1
1319	10	3	6	8386	180	-45	0.4050E-04	0.4079E-04	1.007	L1
1321	10	3	46	8426	176	-38	0.3214E-04	0.3143E-04	0.978	L1
1323	10	3	86	8466	178	-42	0.7631E-04	0.6928E-04	0.908	L1
1324	10	3	106	8486	170	-47	0.1547E-04	0.1733E-04	1.121	L1
1325	10	3	126	8506	354	54	0.6684E-04	0.6042E-04	0.904	L1
1327	10	4	6	8536	299	45	0.4472E-04	0.3356E-04	0.750	L1
1329	10	4	46	8576	311	48	0.6309E-04	0.5494E-04	0.871	L1
1331	10	4	86	8616	318	50	0.6750E-04	0.5654E-04	0.838	L1
1333	10	4	126	8656	307	46	0.6016E-04	0.4713E-04	0.783	L1
1335	10	5	6	8686	297	44	0.6861E-04	0.5820E-04	0.848	L1
1337	10	5	46	8726	294	46	0.5962E-04	0.5166E-04	0.866	L1
1338	10	5	66	8746	294	45	0.2063E-04	0.1487E-04	0.721	L1
1339	10	5	86	8766	123	-44	0.3724E-04	0.3765E-04	1.011	L1
1340	10	5	106	8786	108	-46	0.5225E-04	0.4965E-04	0.950	L1
1341	10	5	126	8806	108	-46	0.3914E-04	0.4185E-04	1.069	L1
1343	10	6	6	8836	76	-47	0.5016E-04	0.4799E-04	0.957	L1
1345	10	6	46	8876	64	-41	0.3957E-04	0.4588E-04	1.159	L1
1347	10	6	86	8916	62	-37	0.4167E-04	0.4665E-04	1.120	L1
1349	11	1	26	9056	199	-54	0.6015E-04	0.5868E-04	0.976	L1
1351	11	1	66	9096	196	-55	0.5362E-04	0.5684E-04	1.060	L1
1353	11	1	106	9136	196	-52	0.5078E-04	0.5196E-04	1.023	L1
1355	11	1	143	9176	192	-49	0.2599E-04	0.2794E-04	1.075	L1
1357	11	2	26	9206	196	-51	0.2544E-04	0.2501E-04	0.983	L1
1359	11	2	66	9246	198	-33	0.3502E-04	0.3362E-04	0.960	L1
1361	11	2	106	9286	200	-45	0.4665E-04	0.4971E-04	1.066	L1
1363	11	2	146	9326	203	-58	0.4504E-04	0.4817E-04	1.069	L1
1364	11	3	6	9336	225	-53	0.3167E-04	0.3390E-04	1.070	L1
1365	11	3	26	9356	26	55	0.4916E-04	0.3987E-04	0.811	L1
1367	11	3	66	9396	22	47	0.4220E-04	0.3502E-04	0.830	L1
1369	11	3	106	9436	17	47	0.6359E-04	0.5831E-04	0.917	L1
1370	11	3	126	9456	14	54	0.3733E-04	0.3120E-04	0.836	L1
1371	11	3	146	9476	200	-29	0.6256E-05	0.7830E-05	1.252	L1
1373	11	4	26	9506	205	-47	0.4083E-04	0.4364E-04	1.069	L1
1375	11	4	66	9546	210	-42	0.2594E-04	0.2678E-04	1.033	L1
1377	11	4	106	9586	208	-52	0.2329E-04	0.2467E-04	1.059	L1
1379	11	4	146	9626	199	-52	0.2965E-04	0.3123E-04	1.053	L1
1380	11	5	6	9636	196	-57	0.8611E-05	0.1054E-04	1.223	L1
1381	11	5	26	9656	42	51	0.2645E-04	0.2101E-04	0.794	L1
1383	11	5	66	9696	42	47	0.3562E-04	0.2986E-04	0.838	L1
1385	11	5	97	9727	41	49	0.4141E-04	0.3415E-04	0.825	L1
1386	11	5	116	9746	85	4	0.8046E-05	0.3718E-05	0.462	A2,4
1387	11	5	134	9764	207	-48	0.4231E-04	0.4279E-04	1.011	L1
1389	11	6	26	9806	228	-53	0.2945E-04	0.3219E-04	1.093	L1
1391	11	6	66	9846	228	-42	0.3202E-04	0.3241E-04	1.012	L1
1393	11	6	106	9886	225	-47	0.4696E-04	0.4246E-04	0.904	L1
1394	11	6	126	9906	217	-44	0.2680E-04	0.2554E-04	0.953	L1
1395	11	6	146	9926	45	56	0.3465E-04	0.2612E-04	0.754	L1
1397	11	7	21	9951	44	45	0.4694E-04	0.3983E-04	0.849	L1
1399	12	1	96	10013	160	32	0.3709E-04	0.3111E-04	0.839	L1
1401	12	1	146	10054	145	36	0.1900E-04	0.1476E-04	0.777	L1
1402	12	2	4	10062	169	28	0.6665E-05	0.4931E-05	0.740	L1
1403	12	2	34	10092	306	-27	0.3246E-04	0.3797E-04	1.170	L1
1405	12	2	67	10125	311	-22	0.8694E-05	0.7190E-05	0.827	A3-4
1407	12	2	106	10164	314	-49	0.2826E-04	0.3213E-04	1.137	L1
1408	12	2	126	10184	142	55	0.3917E-04	0.2985E-04	0.762	L1
1409	12	2	146	10204	142	47	0.5624E-04	0.4447E-04	0.791	L1
1411	12	3	26	10234	133	49	0.4837E-04	0.4022E-04	0.832	L1
1413	12	3	66	10274	136	50	0.4737E-04	0.3580E-04	0.756	L1

Table 6. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	Note
1415	12	3	111	10319	139	52	0.4742E-04	0.3598E-04	0.759	L1
1416	12	4	6	10364	145	44	0.2173E-04	0.1056E-04	0.486	L1
1417	12	4	26	10384	313	-51	0.2152E-04	0.2701E-04	1.255	L1
1419	12	4	66	10424	327	-38	0.2076E-04	0.2413E-04	1.163	L1
1421	12	4	106	10464	307	-58	0.1631E-04	0.2127E-04	1.304	L1
1423	12	4	146	10504	313	-49	0.2302E-04	0.2513E-04	1.092	L1
1425	12	5	26	10534	310	-44	0.1929E-04	0.2299E-04	1.192	L1
1427	12	5	66	10574	320	-51	0.2865E-04	0.3227E-04	1.126	L1
1429	12	5	106	10614	316	-31	0.1219E-04	0.1674E-04	1.373	L1
1431	12	5	146	10654	307	-44	0.1968E-04	0.2228E-04	1.132	L1
1433	12	6	86	10744	289	-52	0.2139E-04	0.2317E-04	1.083	L1
1435	12	6	123	10781	274	-51	0.1586E-04	0.1749E-04	1.103	L1
1437	13	1	26	10956	353	-49	0.8239E-05	0.1239E-04	1.503	L1
1438	13	1	46	10976	159	48	0.3311E-04	0.2597E-04	0.784	L1
1439	13	1	66	10996	168	49	0.3535E-04	0.2780E-04	0.786	L1
1440	13	1	86	11016	164	52	0.4564E-04	0.3470E-04	0.760	L1
1441	13	1	106	11036	156	48	0.2597E-04	0.1777E-04	0.684	L1
1442	13	1	126	11056	161	40	0.3100E-04	0.2218E-04	0.715	L1
1443	13	1	146	11076	169	59	0.1494E-04	0.9174E-05	0.614	L1
1444	13	2	6	11086	154	36	0.2060E-04	0.1534E-04	0.745	L1
1445	13	2	26	11106	160	47	0.3059E-04	0.2351E-04	0.768	L1
1446	13	2	46	11126	165	45	0.3959E-04	0.2761E-04	0.697	L1
1447	13	2	66	11146	167	44	0.3294E-04	0.2547E-04	0.773	L1
1448	13	2	86	11166	159	46	0.3418E-04	0.2715E-04	0.794	L1
1449	13	2	106	11186	172	-60	0.7371E-05	0.1523E-05	0.207	A1-3
1450	13	2	126	11206	340	-51	0.1065E-04	0.1448E-04	1.359	L1
1451	13	2	146	11226	8	-49	0.1968E-04	0.2173E-04	1.104	L1
1452	13	3	6	11236	340	-44	0.1294E-04	0.1516E-04	1.171	L1
1453	13	3	26	11256	3	-33	0.1418E-05	0.3569E-05	2.517	L1
1454	13	3	46	11276	351	-44	0.1449E-04	0.1711E-04	1.181	L1
1455	13	3	66	11296	356	-33	0.9721E-05	0.1608E-04	1.655	L1
1456	13	3	86	11316	358	-47	0.1185E-04	0.1465E-04	1.237	L1
1457	13	3	106	11336	177	32	0.1770E-04	0.9773E-05	0.552	L1
1458	13	3	126	11356	187	44	0.2936E-04	0.1979E-04	0.674	L1
1459	13	3	146	11376	192	47	0.3660E-04	0.2497E-04	0.682	L1
1460	13	4	6	11386	204	51	0.3511E-04	0.2531E-04	0.721	L1
1461	13	4	26	11406	196	45	0.2804E-04	0.2018E-04	0.720	L1
1462	13	4	46	11426	162	-41	0.4035E-04	0.3189E-04	0.790	L1
1463	13	4	66	11446	208	40	0.1956E-04	0.1505E-04	0.769	L1
1464	13	4	86	11466	13	15	0.4203E-05	0.3235E-05	0.770	A1-3
1465	13	4	106	11486	212	47	0.3481E-04	0.2337E-04	0.671	L1
1466	13	4	126	11506	211	45	0.2380E-04	0.1755E-04	0.737	L1
1467	13	4	146	11526	213	49	0.2796E-04	0.1977E-04	0.707	L1
1468	13	5	6	11536	210	46	0.4190E-04	0.3183E-04	0.760	L1
1469	13	5	26	11556	214	49	0.2937E-04	0.2102E-04	0.716	L1
1470	13	5	46	11576	212	41	0.2836E-04	0.1905E-04	0.672	L1
1471	13	5	66	11596	56	64	0.8749E-05	0.2183E-05	0.250	A2-3
1472	13	5	86	11616	35	-43	0.1354E-04	0.1816E-04	1.341	L1
1473	13	5	106	11636	30	-44	0.1729E-04	0.2430E-04	1.405	L1
1474	13	5	126	11656	32	-45	0.1740E-04	0.2217E-04	1.274	L1
1475	13	5	146	11676	24	-39	0.1543E-04	0.1915E-04	1.241	L1
1476	13	6	6	11686	27	-34	0.1514E-04	0.1852E-04	1.223	L1
1477	13	6	26	11706	28	-41	0.1792E-04	0.2364E-04	1.319	L1
1478	13	6	46	11726	30	-45	0.2548E-04	0.2866E-04	1.125	L1
1479	13	6	66	11746	30	-44	0.1807E-04	0.2376E-04	1.315	L1
1480	13	6	86	11766	30	-49	0.1385E-04	0.1780E-04	1.284	L1
1481	13	6	106	11786	16	-44	0.1404E-04	0.2264E-04	1.613	L1
1482	13	6	126	11806	173	-10	0.2589E-05	0.5176E-05	1.999	L1
1483	13	6	146	11826	29	-39	0.1924E-04	0.2846E-04	1.479	L1
1484	13	7	6	11836	27	-47	0.1312E-04	0.1708E-04	1.302	L1

Table 6. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	Note
1485	13	7	26	11856	22	-48	0.1200E-04	0.1936E-04	1.614	L1
1486	14	1	31	11866	189	53	0.2533E-04	0.1723E-04	0.680	L1
1487	14	1	56	11891	246	41	0.4624E-04	0.3475E-04	0.752	L1
1488	14	1	86	11921	36	-60	0.8273E-05	0.1264E-04	1.528	L1
1489	14	1	106	11941	217	46	0.4058E-04	0.2765E-04	0.681	L1
1490	14	1	146	11981	37	-54	0.1463E-05	0.7047E-05	4.817	L1
1491	14	2	6	11991	39	-50	0.1304E-04	0.2080E-04	1.594	L1
1492	14	2	26	12011	33	-46	0.9752E-05	0.1474E-04	1.511	L1
1493	14	2	46	12031	35	-47	0.1231E-04	0.1918E-04	1.558	L1
1494	14	2	66	12051	235	50	0.2119E-04	0.1194E-04	0.563	L1
1495	14	2	86	12071	207	54	0.1477E-04	0.7275E-05	0.493	L1
1496	14	2	106	12091	31	-47	0.9361E-05	0.1369E-04	1.462	L1
1497	14	2	126	12111	210	50	0.2554E-04	0.1493E-04	0.585	L1
1498	14	2	146	12131	208	48	0.3486E-04	0.2417E-04	0.693	L1
1499	14	3	6	12141	215	44	0.4112E-04	0.2663E-04	0.648	L1
1500	14	3	26	12161	21	-45	0.3142E-05	0.8150E-05	2.594	L1
1501	14	3	46	12181	214	45	0.1590E-04	0.7077E-05	0.445	L1
1502	14	3	66	12201	216	48	0.2341E-04	0.1442E-04	0.616	L1
1503	14	3	86	12221	221	46	0.3661E-04	0.2373E-04	0.648	L1
1504	14	3	106	12241	209	48	0.5163E-04	0.4087E-04	0.792	L1
1505	14	3	126	12261	218	45	0.5122E-04	0.3340E-04	0.652	L1
1506	14	3	146	12281	217	49	0.4075E-04	0.2651E-04	0.650	L1
1507	14	4	6	12291	220	40	0.4312E-04	0.3129E-04	0.726	L1
1508	14	4	26	12311	213	47	0.3900E-04	0.3051E-04	0.782	L1
1509	14	4	46	12331	206	47	0.3678E-04	0.2183E-04	0.594	L1
1510	14	4	66	12351	211	37	0.3144E-04	0.2271E-04	0.722	L1
1511	14	4	86	12371	210	42	0.4121E-04	0.2822E-04	0.685	L1
1512	14	4	106	12391	32	-51	0.7912E-05	0.1485E-04	1.877	L1
1513	14	4	126	12411	23	-47	0.6006E-05	0.6313E-05	1.051	L1
1514	14	4	146	12431	8	-43	0.2324E-04	0.2954E-05	0.127	A2-4
1515	14	5	6	12441	238	74	0.3502E-04	0.1038E-04	0.296	L1
1516	14	5	26	12461	200	42	0.3547E-04	0.2018E-04	0.569	L1
1517	14	5	46	12481	24	-40	0.2395E-04	0.3157E-04	1.318	L1
1518	14	5	66	12501	24	-41	0.1698E-04	0.2228E-04	1.312	L1
1519	14	5	86	12521	28	-41	0.2309E-04	0.3141E-04	1.360	L1
1520	14	5	106	12541	21	-41	0.2972E-04	0.3448E-04	1.160	L1
1521	14	5	126	12561	21	-43	0.2532E-04	0.3161E-04	1.248	L1
1522	14	5	146	12581	18	-46	0.2950E-04	0.3579E-04	1.213	L1
1523	14	6	6	12591	18	-39	0.2763E-04	0.3340E-04	1.209	L1
1524	14	6	26	12611	177	46	0.1797E-04	0.9230E-05	0.514	L1
1525	14	6	46	12631	15	-35	0.1206E-04	0.2111E-04	1.750	L1
1526	14	6	66	12651	197	53	0.5247E-04	0.3329E-04	0.634	L1
1527	14	6	86	12671	201	44	0.6367E-04	0.4145E-04	0.651	L1
1528	14	6	106	12691	200	43	0.5489E-04	0.3569E-04	0.650	L1
1529	14	6	126	12711	203	45	0.4876E-04	0.3162E-04	0.649	L1
1530	14	6	138	12723	197	48	0.4790E-04	0.2892E-04	0.604	L1
1531	14	7	6	12741	351	-26	0.9530E-05	0.4193E-05	0.440	L1
1532	14	7	26	12761	31	-38	0.1018E-04	0.2033E-05	0.200	L1
1533	14	7	44	12779	242	47	0.1644E-04	0.2298E-05	0.140	L1
1538	15	1	44	12844	10	35	0.3002E-04	0.1502E-04	0.500	L1
1539	15	1	66	12866	12	50	0.2763E-04	0.1818E-04	0.658	L1
1540	15	1	86	12886	5	46	0.3703E-04	0.2156E-04	0.582	L1
1541	15	1	108	12908	6	48	0.4506E-04	0.3042E-04	0.675	L1
1542	15	1	126	12926	8	38	0.3070E-04	0.1880E-04	0.612	L1
1543	15	1	146	12946	7	44	0.2548E-04	0.1646E-04	0.646	L1
1544	15	2	6	12956	18	45	0.3706E-04	0.2395E-04	0.646	L1
1545	15	2	26	12976	21	40	0.3596E-04	0.2036E-04	0.566	L1
1546	15	2	46	12996	17	43	0.5665E-04	0.3519E-04	0.621	L1
1547	15	2	66	13016	22	44	0.3196E-04	0.2053E-04	0.642	L1
1548	15	2	86	13036	25	43	0.3378E-04	0.1933E-04	0.572	L1

Table 6. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	Note
1549	15	2	106	13056	30	39	0.3428E-04	0.2187E-04	0.638	L1
1550	15	2	126	13076	18	43	0.4259E-04	0.2585E-04	0.607	L1
1551	15	2	146	13096	28	43	0.4667E-04	0.3579E-04	0.767	L1
1552	15	3	6	13106	216	-40	0.9441E-05	0.1392E-04	1.474	L1
1553	15	3	26	13126	215	-45	0.3001E-04	0.3488E-04	1.162	L1
1554	15	3	46	13146	39	39	0.4376E-04	0.3294E-04	0.753	L1
1555	15	3	66	13166	224	-42	0.1235E-04	0.1592E-04	1.289	L1
1556	15	3	86	13186	42	45	0.2121E-04	0.1063E-04	0.501	L1
1557	15	3	106	13206	229	-38	0.4946E-05	0.1014E-04	2.050	L1
1558	15	3	126	13226	223	-39	0.6896E-05	0.1248E-04	1.809	L1
1559	15	3	146	13246	220	-47	0.2387E-04	0.2887E-04	1.210	L1
1560	15	4	6	13256	226	-46	0.1605E-04	0.1657E-04	1.032	L1
1561	15	4	26	13276	228	-46	0.1456E-04	0.1803E-04	1.239	L1
1562	15	4	46	13296	54	47	0.3137E-04	0.2054E-04	0.655	L1
1563	15	4	66	13316	189	-35	0.7430E-05	0.1533E-05	0.206	L1
1564	15	4	86	13336	246	-42	0.3972E-05	0.1167E-04	2.939	L1
1565	15	4	106	13356	231	-42	0.1475E-04	0.2004E-04	1.358	L1
1566	15	4	126	13376	243	-36	0.8419E-05	0.1491E-04	1.771	L1
1567	15	4	146	13396	236	-39	0.7604E-05	0.1191E-04	1.566	L1
1568	15	5	6	13406	244	-41	0.1656E-04	0.2228E-04	1.345	L1
1569	15	5	26	13426	244	-39	0.1789E-04	0.2333E-04	1.304	L1
1570	15	5	46	13446	64	47	0.2998E-04	0.1630E-04	0.544	L1
1571	15	5	66	13466	68	48	0.3657E-04	0.2274E-04	0.622	L1
1572	15	5	84	13484	258	-36	0.4662E-05	0.3502E-05	0.751	L1
1573	15	5	100	13500	248	-46	0.1232E-04	0.1737E-04	1.410	L1
1574	15	5	116	13516	70	42	0.1740E-04	0.6583E-05	0.378	L1
1575	15	6	6	13556	72	43	0.4046E-04	0.2943E-04	0.727	L1
1576	15	6	26	13576	109	13	0.1144E-04	0.3175E-05	0.278	A2-3
1577	15	6	46	13596	241	-42	0.7020E-05	0.9208E-05	1.312	L1
1578	15	6	66	13616	254	-48	0.1224E-04	0.1810E-04	1.479	L1
1579	15	6	86	13636	202	-71	0.1065E-04	0.1399E-04	1.314	L1
1580	15	6	106	13656	249	-43	0.1101E-04	0.1888E-04	1.715	L1
1581	15	6	116	13666	74	51	0.2254E-04	0.1406E-04	0.624	L1
1582	15	6	146	13696	254	-30	0.7919E-05	0.1259E-04	1.591	L1
1583	15	7	6	13706	250	-39	0.7291E-05	0.1148E-04	1.574	L1
1584	15	7	26	13726	65	43	0.3110E-04	0.1872E-04	0.602	L1
1585	15	7	45	13745	137	-72	0.8058E-05	0.4334E-05	0.538	L1
1586	16	1	36	13811	175	-58	0.2041E-04	0.1981E-04	0.971	L1
1587	16	1	56	13831	180	-69	0.1941E-04	0.2104E-04	1.084	L1
1588	16	1	76	13851			0.2368E-04	0.1437E-04	0.607	F
1589	16	1	96	13871			0.1852E-04	0.1454E-04	0.785	F
1590	16	1	116	13891			0.9501E-05	0.7753E-06	0.082	F
1591	16	1	136	13911	127	-36	0.4586E-05	0.1184E-04	2.581	L1
1592	16	2	6	13931	130	-41	0.8434E-05	0.1075E-04	1.274	L1
1593	16	2	26	13951	310	42	0.3245E-04	0.1746E-04	0.538	L1
1594	16	2	46	13971	306	35	0.1881E-04	0.6758E-05	0.359	L1
1595	16	2	66	13991	311	47	0.2391E-04	0.1421E-04	0.595	L1
1596	16	2	86	14011	116	-34	0.5894E-05	0.1342E-04	2.277	L1
1597	16	2	106	14031	115	-39	0.1061E-05	0.9290E-05	8.760	L1
1598	16	2	126	14051	122	-39	0.7173E-05	0.6423E-05	0.895	L1
1599	16	2	146	14071	307	38	0.2429E-04	0.1301E-04	0.536	L1
1600	16	3	6	14081	292	48	0.3254E-04	0.1882E-04	0.578	L1
1601	16	3	26	14101	300	52	0.2697E-04	0.1707E-04	0.633	L1
1602	16	3	46	14121	296	44	0.3104E-04	0.1657E-04	0.534	L1
1603	16	3	66	14141	299	43	0.2920E-04	0.1614E-04	0.553	L1
1604	16	3	86	14161	299	48	0.3069E-04	0.1672E-04	0.545	L1
1605	16	3	106	14181	118	-40	0.4671E-05	0.7214E-05	1.544	L1
1606	16	3	126	14201	295	54	0.2012E-04	0.7350E-05	0.365	L1
1607	16	3	146	14221	304	49	0.3431E-04	0.1978E-04	0.576	L1
1608	16	4	6	14231	288	57	0.3891E-04	0.1945E-04	0.500	L1

Table 6. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	Note
1609	16	4	26	14251	295	49	0.2588E-04	0.1419E-04	0.548	L1
1610	16	4	46	14271	302	52	0.3367E-04	0.1291E-04	0.383	L1
1611	16	4	66	14291	304	47	0.1854E-04	0.8913E-05	0.481	L1
1612	16	4	86	14311	305	53	0.3482E-04	0.2341E-04	0.672	L1
1613	16	4	106	14331	307	55	0.2479E-04	0.1343E-04	0.542	L1
1614	16	4	126	14351	113	-52	0.7806E-05	0.1519E-04	1.946	L1
1615	16	4	146	14371	121	-48	0.5035E-05	0.1095E-04	2.175	L1
1616	16	5	6	14381	122	-39	0.3309E-05	0.7869E-05	2.378	L1
1617	16	5	26	14401	108	-51	0.7526E-05	0.1389E-04	1.845	L1
1618	16	5	46	14421	297	58	0.4191E-04	0.1792E-04	0.428	L1
1619	16	5	66	14441	120	-51	0.9065E-05	0.5156E-05	0.569	L1
1620	16	5	86	14461	264	53	0.3941E-04	0.1885E-04	0.478	L1
1621	16	5	106	14481	295	54	0.3171E-04	0.1877E-04	0.592	L1
1622	16	5	126	14501	90	-56	0.9104E-05	0.1775E-05	0.195	L1
1623	16	5	146	14521	101	-56	0.3760E-05	0.1319E-04	3.507	L1
1624	16	6	7	14532	97	-53	0.2974E-05	0.1194E-04	4.016	L1
1625	16	6	21	14546	120	-55	0.3110E-05	0.8721E-05	2.804	L1
1626	17	1	32	14734	11	-27	0.5588E-05	0.1171E-04	2.096	L1
1627	17	1	48	14750	8	-35	0.3507E-05	0.1355E-04	3.864	L1
1628	17	1	67	14769	358	-27		0.5876E-05		L1
1629	17	1	86	14788	189	41	0.2875E-04	0.8843E-05	0.308	L1
1630	17	1	106	14808	188	32	0.3565E-04	0.1142E-04	0.320	L1
1631	17	1	126	14828	190	35	0.3124E-04	0.1310E-04	0.419	L1
1632	17	1	146	14848	8	-23	0.1519E-04	0.3254E-05	0.214	L1
1633	17	2	11	14863	28	-23	0.1430E-04	0.4898E-05	0.342	L1
1634	17	2	43	14895	208	41	0.2591E-04	0.7429E-05	0.287	L1
1635	17	2	55	14907	209	33	0.3334E-04	0.1251E-04	0.375	L1
1636	17	2	71	14923	209	34	0.2936E-04	0.7848E-05	0.267	L1
1637	17	2	86	14938	212	31	0.3446E-04	0.1332E-04	0.386	L1
1638	17	2	106	14958	216	32	0.3100E-04	0.8913E-05	0.288	L1
1639	17	2	116	14978	213	36	0.2674E-04	0.7604E-05	0.284	L1
1640	17	2	146	14998	24	-37	0.1304E-04	0.4397E-05	0.337	L1
1641	17	3	6	15008	35	- 4	0.1532E-04	0.2212E-05	0.144	L1
1642	17	3	26	15028	36	-26	0.9142E-05	0.4795E-05	0.525	L1
1643	17	3	46	15048	223	39	0.2501E-04	0.7120E-05	0.285	L1
1644	17	3	66	15068	224	69	0.2510E-04	0.1935E-05	0.077	L1
1645	17	3	82	15084	230	39	0.2861E-04	0.4050E-05	0.142	L1
1646	17	3	99	15101	222	26	0.2749E-04	0.2729E-05	0.099	L1
1647	17	3	118	15120	221	57	0.2796E-04	0.2341E-05	0.084	L1
1648	17	3	134	15136	236	68	0.2665E-04	0.2439E-05	0.092	L1
1649	17	4	6	15158			0.2442E-04			
1650	17	4	26	15178	80	53	0.3638E-04	0.2573E-05	0.071	L1
1651	17	4	46	15198	66	38	0.3047E-04	0.4412E-05	0.145	L1
1652	17	4	66	15218	65	44	0.3240E-04	0.4173E-05	0.129	L1
1653	17	4	82	15234	60	40	0.4795E-04	0.9313E-05	0.194	L1
1654	17	4	100	15252	52	50	0.5287E-04	0.8289E-05	0.157	L1
1655	17	4	118	15270	227	-53	0.2877E-04	0.4426E-05	0.154	L1
1656	17	4	136	15288	65	44	0.3212E-04	0.7608E-05	0.237	L1
1657	17	5	6	15308	161	-41	0.3230E-04	0.1493E-05	0.046	L1
1658	17	5	26	15328	26	43	0.4083E-04	0.5451E-05	0.134	L1
1659	17	5	46	15348	170	-61	0.4079E-04	0.1871E-05	0.046	L1
1660	17	5	66	15368	26	47	0.5119E-04	0.3999E-04	0.781	L1
1661	17	5	86	15388	77	- 3	0.3779E-04	0.9297E-06	0.025	L1
1662	17	5	106	15408	32	30	0.3819E-04	0.6601E-05	0.173	L1
1663	17	5	126	15428	29	38	0.4074E-04	0.6990E-05	0.172	L1
1664	18	1	26	15686	108	19	0.3434E-04	0.1357E-04	0.395	L1
1665	18	1	46	15706	127	30	0.3803E-04	0.1626E-04	0.428	L1
1666	18	1	66	15726	294	-38	0.1403E-04	0.9060E-05	0.646	L1
1667	18	1	86	15746	292	-35	0.1273E-04	0.1168E-04	0.918	L1
1668	18	1	106	15766	69	-62	0.2475E-04	0.7350E-06	0.030	L1

Table 6. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Declination (deg)	Inclination (deg)	NRM (emu)	J_{100} (emu)	J_{100}/J_0	Note
1669	18	1	126	15786	123	56	0.3054E-04	0.3829E-05	0.125	L1
1670	18	1	146	15806	273	-32	0.2734E-04	0.1124E-05	0.041	L2
1671	18	2	6	15816	109	55	0.2195E-04	0.2413E-05	0.110	L1
1672	18	2	29	15839	279	-26	0.2490E-04	0.1746E-05	0.070	L1
1673	18	2	46	15856	112	44	0.4851E-04	0.1534E-04	0.316	L1
1674	18	2	66	15876	285	-39	0.1673E-04	0.9543E-05	0.570	L1
1675	18	2	86	15896	280	-29	0.0000E+00	0.2565E-04	0.000	L1
1676	18	2	106	15916	284	-28	0.1403E-04	0.1146E-04	0.816	L1
1677	18	2	126	15936	290	-48	0.1991E-04	0.2438E-05	0.122	L1
1678	18	2	146	15956	102	35	0.4185E-04	0.9439E-05	0.226	L1
1679	18	3	6	15966	104	29	0.5050E-04	0.2155E-04	0.427	L1
1680	18	3	26	15986	95	29	0.4334E-04	0.1840E-04	0.425	L1
1681	18	3	46	16006	93	43	0.3608E-04	0.1092E-04	0.303	L1
1682	18	3	66	16026	101	36	0.4690E-04	0.1932E-04	0.412	L1
1683	18	3	86	16046	267	15	0.2479E-04	0.5041E-05	0.203	L1
1684	18	3	106	16066	99	26	0.4028E-04	0.9549E-05	0.237	L1
1685	18	3	117	16077	307	-46	0.2291E-04	0.2266E-05	0.099	L1
1686	18	4	6	16116	293	-31	0.3353E-04	0.1276E-05	0.038	L2
1687	18	4	26	16136	5	-61	0.3110E-04	0.3020E-05	0.097	L2
1688	18	4	46	16156	309	1	0.2732E-04	0.1373E-05	0.050	A2-8
1689	18	4	66	16176	260	-54	0.2371E-04	0.7729E-05	0.326	L1
1690	18	4	86	16196	107	57	0.3912E-04	0.5386E-05	0.138	L1
1691	18	4	106	16216	272	-11	0.2585E-04	0.1773E-05	0.069	L2
1692	18	4	126	16236	288	-15	0.4435E-04	0.1109E-05	0.025	A2,2,3
1693	18	*	5	16248	27	30	0.3709E-04	0.3847E-05	0.104	L1
1694	18	*	30	16273	354	36	0.4899E-04	0.1875E-04	0.383	L1
1695	19	1	47	16634	54	-38	0.2905E-04	0.1927E-04	0.663	L1
1696	19	1	66	16653	196	-68	0.1914E-04	0.4100E-05	0.214	L1
1697	19	1	86	16673	225	-28	0.2365E-04	0.6389E-05	0.270	L1
1698	19	1	106	16693	254	-18	0.3959E-04	0.1108E-05	0.028	L2
1699	19	1	126	16713	87	31	0.3263E-04	0.2728E-05	0.084	L1
1700	19	1	146	16733	66	38	0.5360E-04	0.1249E-04	0.233	L1
1741	19	2	32	16769	134	-58	0.3322E-04	0.3195E-05	0.096	L1
1742	19	2	48	16785	220	-24	0.3112E-04	0.1861E-04	0.598	L1
1743	19	2	66	16803	61	37	0.7116E-04	0.2620E-04	0.368	L1
1744	19	2	86	16823	73	52	0.5539E-04	0.1618E-04	0.292	L1
1701	19	2	99	16836	58	38	0.6668E-04	0.2130E-04	0.319	L1
1702	19	2	111	16848	236	-24	0.3478E-04	0.3144E-05	0.090	A2-3
1703	19	2	125	16862	67	50	0.4658E-04	0.9889E-05	0.212	L1
1704	19	2	138	16875	53	40	0.6065E-04	0.1456E-04	0.240	L1
1705	19	3	6	16893	65	60	0.5155E-04	0.8085E-05	0.157	L1
1706	19	3	26	16913	40	48	0.6502E-04	0.1873E-04	0.288	L1
1707	19	3	46	16933	40	42	0.5965E-04	0.1962E-04	0.329	L1
1708	19	3	66	16953	58	45	0.7369E-04	0.1264E-04	0.172	L1
1709	19	3	86	16973	36	52	0.1058E-03	0.4526E-04	0.428	L1
1710	19	3	106	16993	48	47	0.7406E-04	0.2157E-04	0.291	L1
1711	19	*	5	17012	131	38	0.6046E-04	0.2648E-04	0.438	L1
1712	19	*	29	17036	335	-51	0.7116E-04	0.2450E-04	0.344	L1
1534	20	1	6	17586	21	-60	0.3479E-04	0.2473E-04	0.711	L1
1535	20	1	22	17602	85	-82	0.2995E-04	0.2995E-04	1.000	L1
1536	20	1	46	17626	19	- 2	0.4952E-04	0.6246E-05	0.126	L1
1537	20	1	71	17651	170	-59	0.3531E-04	0.7584E-05	0.215	L1

Note: A = vector average of declination and inclination at demagnetization levels (x100) shown. L = demagnetization level (x 100) used to define declination and inclination.
F = flow-material (based on shipboard visual descriptions).

Table 7. Magnetization of Site 578 samples after AF demagnetization at intensities above 100 Oe.

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Demagnetization Level (OE)	J (emu)	J/J_0
932	2	1	146	626	200	0.4132E-04	0.695
					300	0.2687E-04	0.452
					400	0.1937E-04	0.326
933	2	2	5	635	200	0.2073E-04	0.604
					300	0.1406E-04	0.410
934	2	2	26	656	200	0.3296E-04	0.623
					300	0.2351E-04	0.444
					400	0.1602E-04	0.303
943	2	3	66	846	200	0.3776E-04	0.615
970	3	1	106	1536	200	0.2907E-04	0.604
					300	0.1972E-04	0.410
					400	0.1318E-04	0.274
971	3	1	126	1556	200	0.2268E-04	0.590
					300	0.1500E-04	0.391
					400	0.1078E-04	0.281
972	3	1	146	1576	200	0.3206E-04	0.643
					300	0.2194E-04	0.440
					400	0.1430E-04	0.287
980	3	2	146	1726	200	0.3292E-04	0.564
					300	0.2160E-04	0.370
					400	0.1529E-04	0.262
981	3	3	6	1736	200	0.3145E-04	0.598
					300	0.2066E-04	0.393
					400	0.1282E-04	0.244
982	3	3	26	1756	200	0.5557E-04	0.643
					300	0.3565E-04	0.413
					400	0.2460E-04	0.285
1015	4	1	26	2406	200	0.5280E-05	0.566
					300	0.3119E-05	0.334
					400	0.1905E-05	0.204
1043	4	3	105	2785	200	0.8119E-05	1.255
					300	0.6588E-05	1.019
1033	4	4	65	2895	200	0.4803E-06	0.931
					300	0.4005E-06	0.776
					400	0.3983E-06	0.772
1035	4	4	110	2940	200	0.7180E-06	0.757
					300	0.6649E-06	0.701
					400	0.4490E-06	0.473
1057	4	6	66	3196	200	0.2376E-04	0.870
					300	0.1644E-04	0.602
1062	5	1	106	3436	200	0.8516E-05	0.441
1079	5	3	128	3758	200	0.8811E-05	0.404
					300	0.6265E-05	0.287
					400	0.3528E-05	0.162
1080	5	3	146	3776	200	0.4987E-05	0.123
					300	0.4579E-05	0.113
					400	0.3042E-05	0.075
					401	0.2945E-05	0.073
					500	0.2658E-05	0.066
					600	0.1237E-05	0.031
1107	6	1	6	4286	200	0.2013E-05	0.441
					300	0.1515E-05	0.332
1129	6	3	146	4726	200	0.5970E-06	0.873
					300	0.4529E-06	0.662
1160	7	1	146	5366	200	0.2766E-04	0.755
					300	0.1873E-04	0.511
1161	7	2	6	5376	200	0.2213E-04	0.674
					300	0.1601E-04	0.487

Table 7. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Demagnetization Level (OE)	J (emu)	J/J_0
1187	7	5	46	5866	200	0.1821E-04	1.534
1203	8	1	26	6206	200	0.1086E-04	0.722
					300	0.6289E-05	0.418
					400	0.3930E-05	0.261
1204	8	1	46	6226	200	0.9682E-06	0.868
1258	9	1	86	7216	200	0.4474E-04	0.786
					300	0.3401E-04	0.598
					400	0.2137E-04	0.376
					500	0.1347E-04	0.237
					600	0.9747E-05	0.171
					700	0.6455E-05	0.113
					800	0.4818E-05	0.085
					900	0.3515E-05	0.062
					1000	0.1613E-04	0.284
					1001	0.2339E-04	0.411
1261	9	1	146	7276	200	0.2555E-04	0.578
					300	0.1791E-04	0.405
					400	0.1125E-04	0.254
1277	9	3	146	7576	200	0.9401E-05	0.595
					300	0.7193E-05	0.456
					400	0.5297E-05	0.335
1281	9	4	66	7646	200	0.5498E-04	0.720
					300	0.3802E-04	0.498
					400	0.2789E-04	0.365
1303	9	7	6	8078	200	0.9738E-05	0.824
1386	11	4	86	9746	200	0.1749E-05	0.217
					400	0.5929E-06	0.074
1402	12	2	4	10062	200	0.3298E-05	0.495
1403	12	2	34	10092	200	0.2829E-04	0.872
1405	12	2	67	10125	200	0.7830E-05	0.901
					300	0.6293E-05	0.724
					400	0.4484E-05	0.516
1449	13	2	106	11186	200	0.9654E-06	0.131
					300	0.7596E-06	0.103
1453	13	3	6	11256	200	0.3595E-05	2.535
					300	0.3129E-05	2.207
1462	13	4	46	11426	200	0.2352E-04	0.583
					201	0.2211E-04	0.548
					300	0.1453E-04	0.360
					400	0.1051E-04	0.260
1464	13	4	86	11466	200	0.2320E-05	0.552
					300	0.1696E-05	0.403
					400	0.1069E-05	0.254
					401	0.1206E-05	0.287
					500	0.8130E-06	0.193
					500	0.8707E-06	0.207
1471	13	5	6	11596	200	0.1755E-05	0.201
					300	0.9173E-06	0.105
1488	14	1	86	11921	200	0.9574E-05	1.157
					300	0.6095E-05	0.737
1490	14	1	146	11981	200	0.5393E-05	3.686
1500	14	3	26	12161	200	0.6505E-05	2.071
1513	14	4	126	12411	200	0.5417E-05	0.902
1514	14	4	146	12431	200	0.2876E-05	0.124
					400	0.2151E-05	0.093
					401	0.1955E-05	0.084
1515	14	5	6	12441	200	0.3592E-05	0.103
					300	0.1548E-05	0.044

Table 7. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Demagnetization Level (OE)	J (emu)	J/J_0
1524	14	6	26	12611	200	0.4682E-05	0.261
1531	14	7	6	12741	200	0.3566E-05	0.374
1532	14	7	26	12761	200	0.2050E-05	0.201
1538	15	1	44	12844	200	0.1030E-04	0.343
1554	15	3	46	13146	200	0.2130E-04	0.487
1557	15	3	106	13206	200	0.7991E-05	1.616
1563	15	4	66	13316	200	0.2058E-05	0.277
1566	15	4	126	13376	200	0.1473E-04	1.749
1567	15	4	146	13396	200	0.9878E-05	1.299
1572	15	5	84	13484	200	0.2857E-05	0.613
1576	15	6	26	13576	200	0.1087E-05	0.095
					300	0.8085E-06	0.071
					400	0.3896E-06	0.034
1577	15	6	46	13596	200	0.7011E-05	0.999
1579	15	6	86	13636	200	0.9886E-05	0.928
					300	0.5618E-05	0.528
					400	0.3977E-05	0.373
1582	15	6	146	13696	200	0.8980E-05	1.134
1585	15	7	45	13745	200	0.3341E-05	0.415
					300	0.2223E-05	0.276
					400	0.1102E-05	0.137
					500	0.9358E-06	0.116
1586	16	1	36	13811	200	0.1333E-04	0.653
1587	16	1	56	13831	200	0.1439E-04	0.741
					300	0.7812E-05	0.402
1590	16	1	116	13891	200	0.3516E-06	0.037
1592	16	2	6	13931	200	0.8549E-05	1.014
1596	16	2	86	14011	200	0.9364E-05	1.589
1597	16	2	106	14031	200	0.7786E-05	7.340
1605	16	3	105	14181	200	0.5042E-05	1.079
1616	16	5	6	14381	200	0.6133E-05	1.854
1619	16	5	66	14441	200	0.4128E-05	0.455
1622	16	5	126	14501	200	0.2322E-05	0.255
					300	0.1419E-05	0.156
					400	0.1134E-05	0.125
1624	16	6	7	14532	200	0.7615E-05	2.560
1625	16	6	21	14546	200	0.6492E-05	2.087
1626	17	1	32	14734	200	0.7998E-05	1.431
					300	0.5865E-05	1.050
1627	17	1	48	14750	200	0.9433E-05	2.689
1628	17	1	67	14769	200	0.4391E-05	
1632	17	1	146	14848	200	0.3200E-05	0.211
1633	17	2	6	14863	200	0.3618E-05	0.253
					300	0.2515E-05	0.176
1635	17	2	55	14907	200	0.7296E-05	0.219
1637	17	2	86	14938	200	0.7611E-05	0.221
1640	17	2	146	14998	200	0.3495E-05	0.268
1641	17	3	6	15008	200	0.1972E-05	0.129
1642	17	3	26	15028	200	0.4236E-05	0.463
1644	17	3	66	15068	200	0.4656E-06	0.019
1646	17	3	99	15101	200	0.6381E-06	0.023
1648	17	3	134	15136	200	0.8466E-06	0.032
1649	17	4	6	15158	200	0.8036E-06	0.033
1651	17	4	46	15198	200	0.1333E-05	0.044
1655	17	4	118	15270	200	0.4578E-05	0.159
1656	17	4	136	15288	200	0.3553E-05	0.111
1657	17	5	6	15308	200	0.2679E-05	0.083
1659	17	5	46	15348	200	0.3254E-05	0.080

Table 7. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Demagnetization Level (OE)	J (emu)	J/J_0
1660	17	5	66	15368	200	0.7063E-05	0.138
1661	17	5	86	15388	200	0.1627E-05	0.043
1664	18	1	26	15686	200	0.7207E-05	0.210
					300	0.4591E-05	0.134
					400	0.2686E-05	0.078
1666	18	1	66	15726	200	0.7451E-05	0.531
1670	18	1	146	15806	200	0.1248E-05	0.046
					300	0.8684E-06	0.032
1672	18	2	29	15839	200	0.2420E-05	0.097
					300	0.2190E-05	0.088
1674	18	2	66	15876	200	0.8124E-05	0.486
1675	18	2	86	15896	200	0.1892E-04	0.000
1676	18	2	106	15916	200	0.9851E-05	0.702
1677	18	2	126	15936	200	0.3407E-05	0.171
1680	18	3	26	15986	200	0.1291E-04	0.298
					300	0.6404E-05	0.148
1682	18	3	66	16026	200	0.1205E-04	0.257
1683	18	3	86	16046	200	0.3223E-05	0.130
					201	0.3684E-05	0.149
					300	0.1944E-05	0.078
					400	0.1801E-05	0.073
					500	0.2234E-05	0.090
					600	0.2448E-05	0.099
1684	18	3	106	16066	200	0.4631E-05	0.115
1685	18	3	117	16077	200	0.2795E-05	0.122
1686	18	4	6	16116	200	0.1562E-05	0.047
1687	18	4	26	16136	200	0.1360E-05	0.044
					201	0.1098E-05	0.035
1688	18	4	46	16156	200	0.1122E-05	0.041
					201	0.1096E-05	0.040
					300	0.1169E-05	0.043
					400	0.2011E-05	0.074
					500	0.1770E-05	0.065
					600	0.3131E-05	0.115
					700	0.2435E-05	0.089
					800	0.2655E-05	0.097
1689	18	4	66	16176	200	0.5579E-05	0.235
1690	18	4	86	16196	200	0.2713E-05	0.069
1691	18	4	106	16216	200	0.2695E-05	0.104
					201	0.2972E-05	0.115
					300	0.1169E-05	0.045
1692	18	4	126	16236	200	0.1328E-05	0.030
					200	0.1290E-05	0.029
1693	18	*	5	16248	200	0.4618E-05	0.125
					201	0.4476E-05	0.121
					300	0.1837E-05	0.050
1694	18	*	30	16273	200	0.1270E-04	0.259
					300	0.7325E-05	0.150
					400	0.3993E-05	0.082
					500	0.2557E-05	0.052
					600	0.2264E-05	0.046
1696	19	1	47	16653	200	0.2600E-05	0.136
					300	0.1071E-05	0.056
1697	19	1	86	16673	200	0.5269E-05	0.223
1698	19	1	106	16693	200	0.2138E-05	0.054
1741	19	2	32	16769	200	0.3776E-05	0.114
1743	19	2	66	16803	200	0.1326E-04	0.186
1702	19	2	111	16848	200	0.4169E-05	0.120

Table 7. (Continued).

Sample	Core	Section	Depth in Section (cm)	Depth in Hole (cm)	Demagnetization Level (OE)	J (emu)	J/J0
					300	0.2160E-05	0.062
1534	20	1	6	17586	200	0.1453E-04	0.418
1535	20	1	22	17602	200	0.1834E-04	0.612
					300	0.9067E-05	0.303
					400	0.4177E-05	0.139
					500	0.3763E-05	0.126
1536	20	1	46	17626	200	0.2795E-05	0.056
					300	0.1223E-05	0.025
1537	20	1	71	17651	200	0.6546E-05	0.185

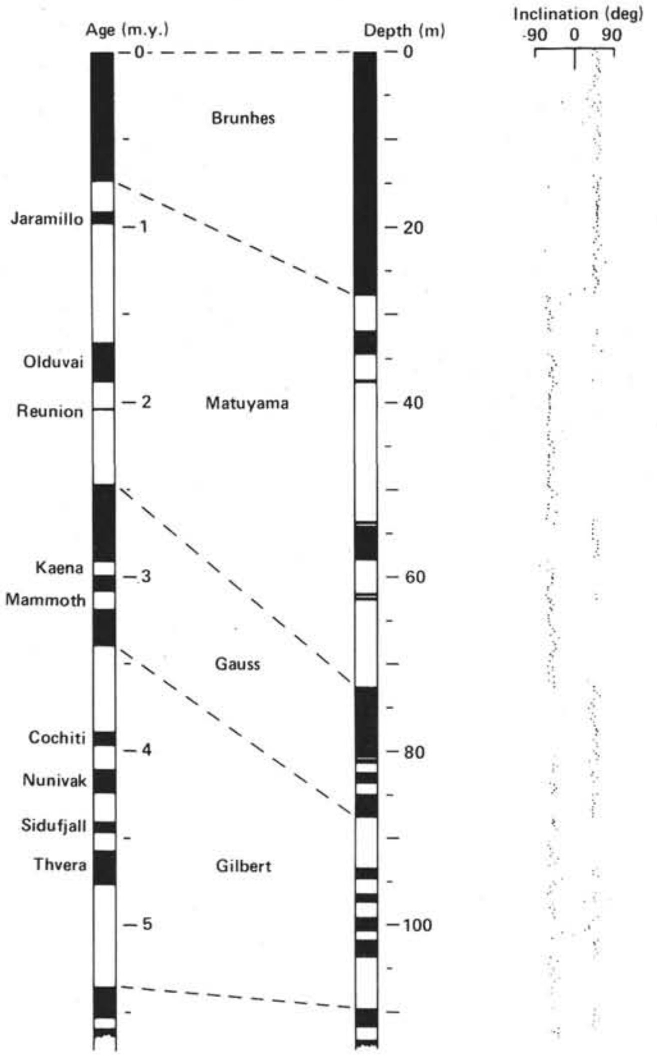

Figure 6. Correlations of the inclination data and paleomagnetic polarity stratigraphy of the upper part of Site 578 with the time scale of Berggren et al. (in press) and the age of the Reunion Event from MacDougall (1977).

Table 8. Magnetostratigraphy for Hole 578.

Age[a] (m.y.)	Depth in hole (m)	Note[b]	Boundary or event
0.73	27.86 ± 0.19		Brunhes/Matuyama
0.91	31.86 ± 0.09		Jaramillo
0.98	34.46 ± 0.09		
	37.46 ± 0.10	(+)[c]	
	37.67 ± 0.08		
1.66	53.56 ± 0.09		
	53.07 ± 0.20	(−)[c]	Olduvai
	54.07 ± 0.09		
1.88	58.06 ± 0.09		
2.01[d]	61.86 ± 0.19		
	62.16 ± 0.09	(−)[c]	Reunion
	62.36 ± 0.09		
2.04[d]	62.56 ± 0.09		
2.47	72.66 ± 0.09		Matuyama/Gauss
	80.67 ± 0.10	(−)[c]	
	80.93 ± 0.14		
2.92	81.43 ± 0.15		Kaena
2.99	82.45 ± 0.08		
3.08	83.66 ± 0.09		Mammoth
3.18	84.96 ± 0.09		
3.40	87.56 ± 0.09		Gauss/Gilbert
3.88	93.46 ± 0.09		Cochiti
3.97	94.66 ± 0.09		
4.10	96.46 ± 0.09		Nunivak
4.24	97.46 ± 0.18		
4.40	99.16 ± 0.09		Sidufjall
4.47	100.77 ± 0.14		
4.57	101.74 ± 0.09		Thvera
4.77	103.74 ± 0.09		
5.35	109.66 ± 0.09		Base of Gilbert
	111.76 ± 0.09		Anomaly 3.1
5.68	113.26 ± 0.09		
	114.16 ± 0.09	(−)[c]	Anomaly 3.2
5.89	115.96 ± 0.19		
6.37	118.61 ± 0.04		
	119.06 ± 0.14	(−)[c]	Anomaly 3.3
	119.31 ± 0.09	(+)	
6.50	119.61 ± 0.19		
6.70	120.41 ± 0.09		
6.78	120.81 ± 0.09	(−)	
6.85	121.01 ± 0.09		
	121.51 ± 0.09	(−)[c]	Anomaly 4
	121.71 ± 0.09		
7.28	123.81 ± 0.09		
7.35	124.36 ± 0.04		
7.41	124.71 ± 0.09		
7.90	126.01 ± 0.09		
	126.21 ± 0.09	(−)[c]	Anomaly 4.1
8.21, 8.80	127.32 ± 0.08		
8.92	127.70 ± 0.08		Anomaly 5
10.42	131.01 ± 0.04		
10.54	131.36 ± 0.09	(+)	Anomaly 5′
10.59	131.56 ± 0.09		
	131.76 ± 0.09	(−)	
	131.96 ± 0.09	(+)[c]	
11.03	132.86 ± 0.09	(+)	
11.09	133.06 ± 0.09		
11.55	134.36 ± 0.09		
11.73	134.75 ± 0.09		
11.86	135.08 ± 0.07		Anomaly 5A
12.12	135.86 ± 0.09		
12.46	136.61 ± 0.04	(+)	
12.49	136.81 ± 0.14		
12.58	137.16 ± 0.09	(+)	
12.62	137.36 ± 0.09		
12.83	138.41 ± 0.09		
13.01	139.01 ± 0.09		
13.20	139.41 ± 0.09		
13.46	140.01 ± 0.09		
13.69	140.61 ± 0.09		
14.08	141.71 ± 0.09	(−)	
14.20	141.91 ± 0.09		
14.66	143.41 ± 0.09		
14.87	144.11 ± 0.09		
14.96	144.31 ± 0.09	(−)	Anomaly 5B
15.13	144.51 ± 0.09		
15.27	144.91 ± 0.09		

[a] From Berggren et al. (in press).
[b] (+) or (−) indicate normal or reversed intervals defined by single samples.
[c] Polarity interval not shown by Berggren et al. (in press).
[d] Reunion age from MacDougall (1977).

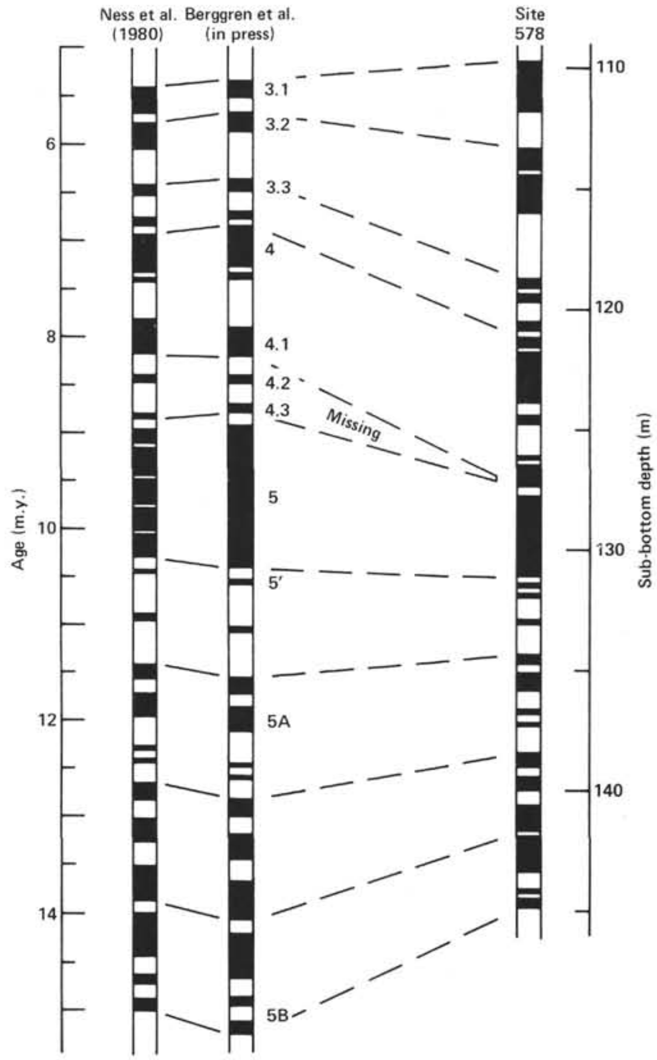

Figure 7. Correlation of the paleomagnetic polarity stratigraphy of the deeper part of Site 578 with the scales of Berggren et al. (in press) and Ness et al. (1980) and marine magnetic Anomalies 3.1 to 5B.

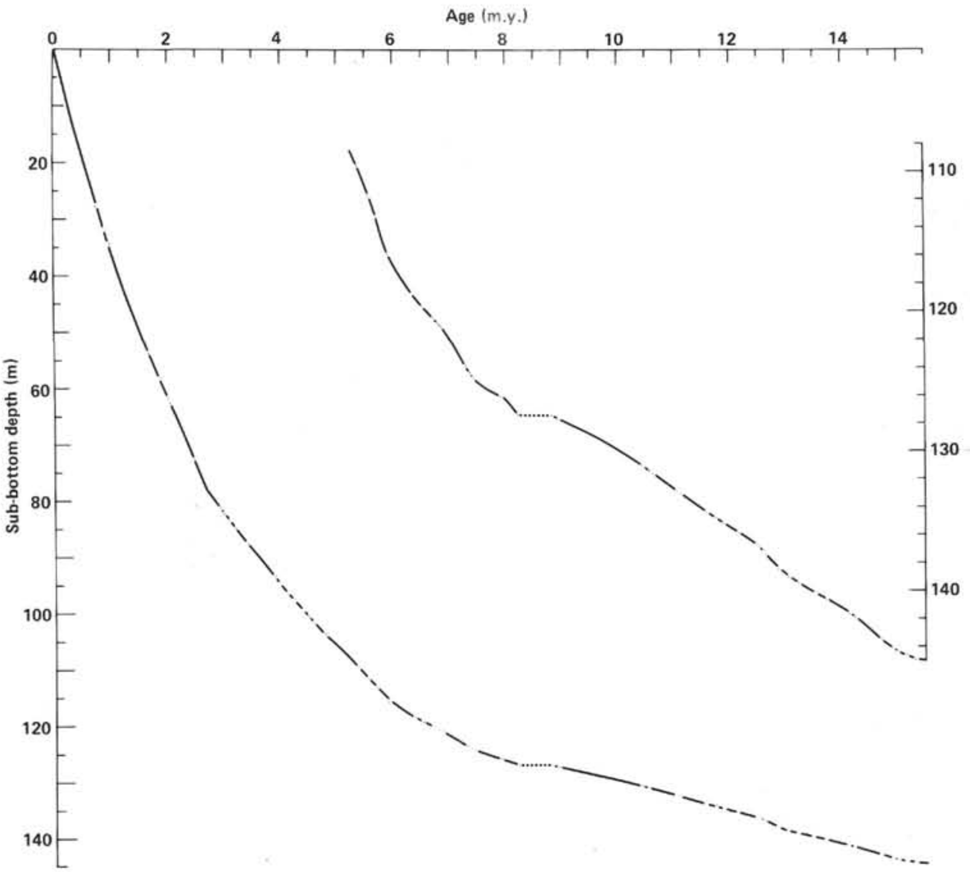

Figure 8. Age-depth curve for Site 578 based on the paleomagnetic correlations of Figures 6 and 7 and the time scale of Berggren et al. (in press). The vertical scale of the 5- to 15-m.y. section (right curve and axis) have been enlarged to show the sedimentation rate changes in more detail.

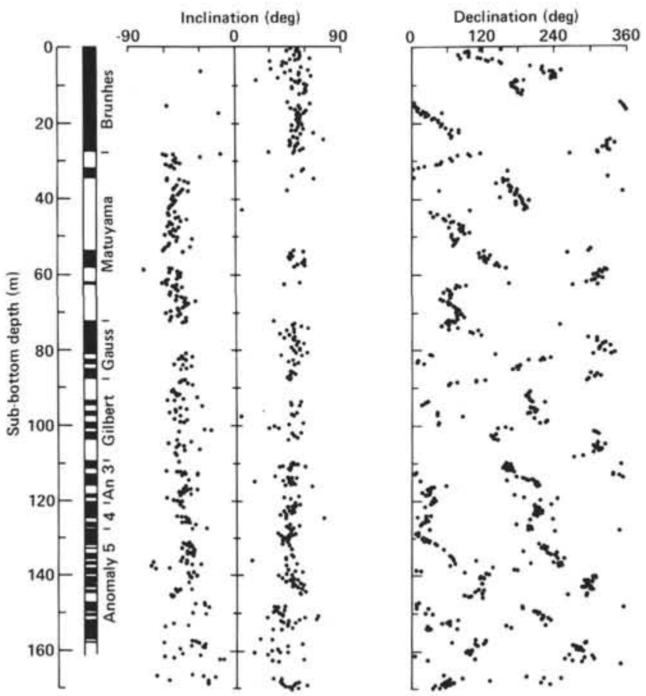

Figure 9. Inclination and declination as a function of depth at Site 578. Rotation of the hydraulic piston core as it cores the sediment is apparent in the declinations for the upper part of the section.

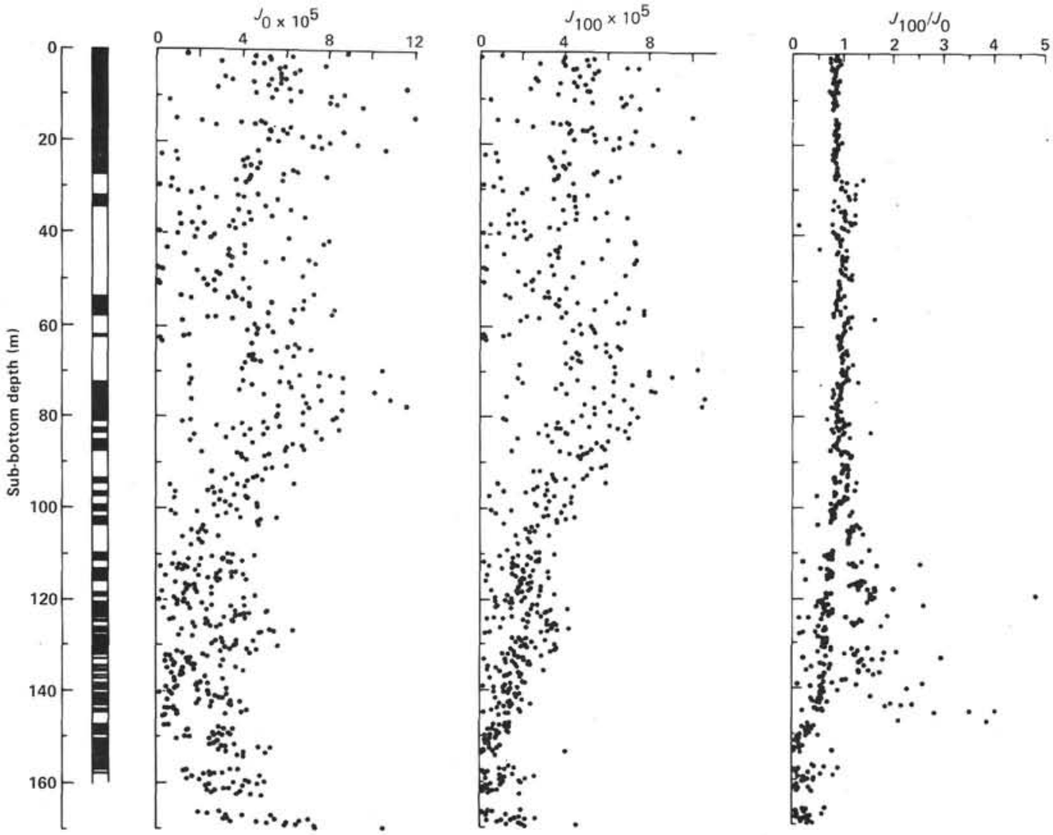

Figure 10. Natural remanent magnetization (J_0), remanent intensity after AF demagnetization at 100 Oe (J_{100}), and J_{100}/J_0 as a function of sub-bottom depth at Site 578.

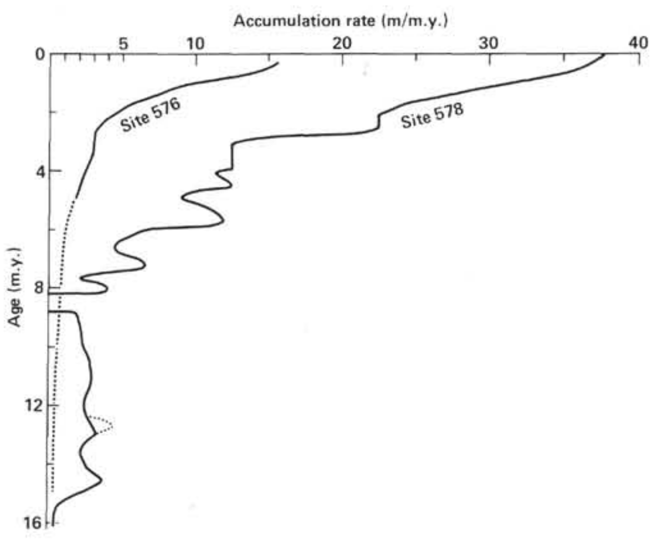

Figure 11. Sediment-accumulation rate as a function of age for the 0- to 16-m.y. sections of Sites 576 and 578. These profiles are obtained by differentiating the curves of Figures 2 and 8 against age. Note the similar rates below 16 m.y. and the similar Quaternary rate accelerations at the two sites. The dotted peak at 12.5 m.y. on the Site 578 curve is believed to be an artifact caused by stretching of the sediment section during the coring process.